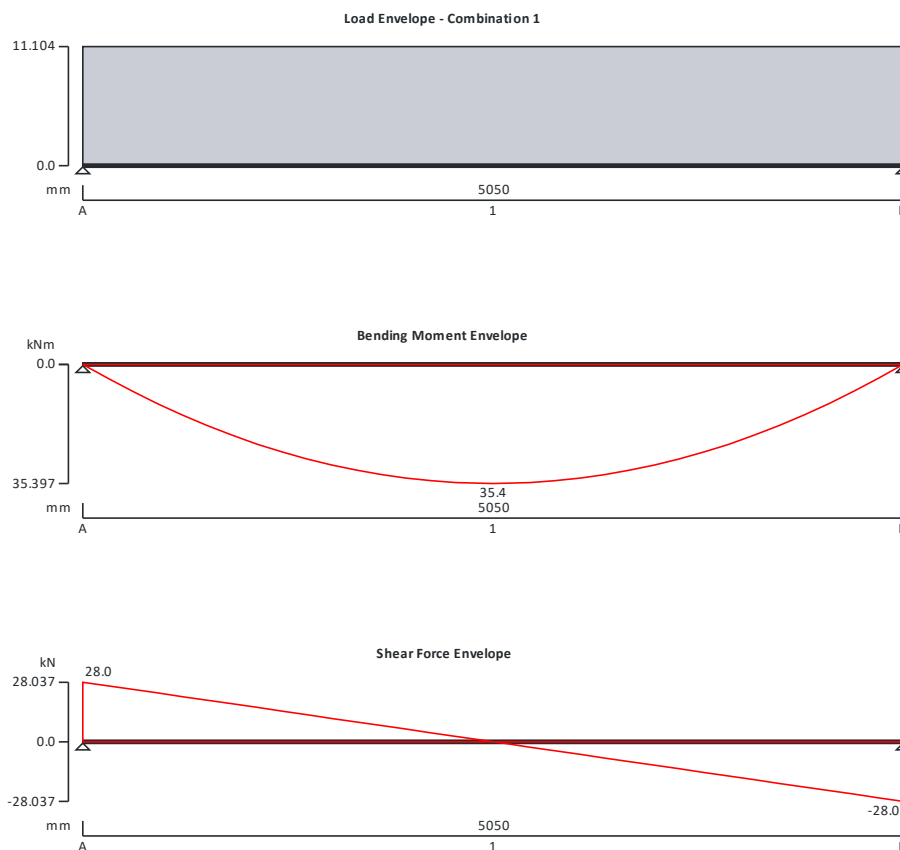


Project 47a NORTH ROAD - BEAM A				Job no. AB/10201	
Calcs for LEWIS WILLETTTS				Start page no./Revision 1 A	
Calcs by AB	Calcs date 24/01/2024	Checked by DC	Checked date 11/01/2024	Approved by DC	Approved date 11/01/2024

STEEL BEAM ANALYSIS & DESIGN (EN1993-1-1:2005)

In accordance with EN1993-1-1:2005 incorporating Corrigenda February 2006 and April 2009 and the UK national annex

TEDDS calculation version 3.0.14



Support conditions

Support A

Vertically restrained

Rotationally free

Support B

Vertically restrained

Rotationally free

Applied loading

Beam loads

Permanent self weight of beam $\times 1$

FLOOR - Permanent full UDL 4 kN/m

ROOF - Permanent full UDL 4 kN/m

Load combinations

Load combination 1

Support A

Permanent $\times 1.35$

Variable $\times 1.50$

Permanent $\times 1.35$

Variable $\times 1.50$

Support B

Permanent $\times 1.35$

Variable $\times 1.50$

Project 47a NORTH ROAD - BEAM A				Job no. AB/10201	
Calcs for LEWIS WILLETTS				Start page no./Revision 2 A	
Calcs by AB	Calcs date 24/01/2024	Checked by DC	Checked date 11/01/2024	Approved by DC	Approved date 11/01/2024

Analysis results

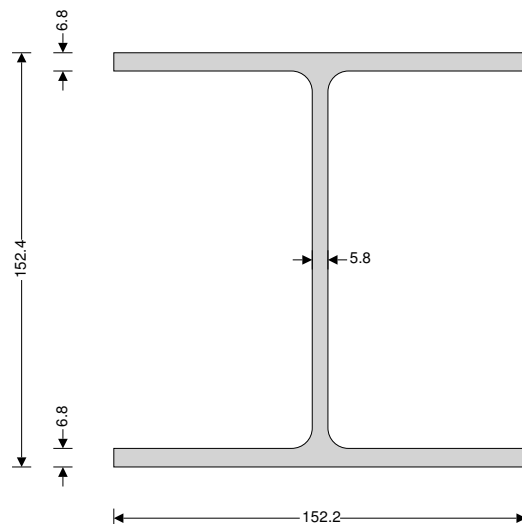
Maximum moment	$M_{\max} = 35.4 \text{ kNm}$	$M_{\min} = 0 \text{ kNm}$
Maximum shear	$V_{\max} = 28 \text{ kN}$	$V_{\min} = -28 \text{ kN}$
Deflection	$\delta_{\max} = 0 \text{ mm}$	$\delta_{\min} = 0 \text{ mm}$
Maximum reaction at support A	$R_{A_{\max}} = 28 \text{ kN}$	$R_{A_{\min}} = 28 \text{ kN}$
Unfactored permanent load reaction at support A	$R_{A_{\text{Permanent}}} = 20.8 \text{ kN}$	
Maximum reaction at support B	$R_{B_{\max}} = 28 \text{ kN}$	$R_{B_{\min}} = 28 \text{ kN}$
Unfactored permanent load reaction at support B	$R_{B_{\text{Permanent}}} = 20.8 \text{ kN}$	

Section details

Section type	UC 152x152x23 (BS4-1)
Steel grade	S275

EN 10025-2:2004 - Hot rolled products of structural steels

Nominal thickness of element	$t = \max(t_f, t_w) = 6.8 \text{ mm}$
Nominal yield strength	$f_y = 275 \text{ N/mm}^2$
Nominal ultimate tensile strength	$f_u = 410 \text{ N/mm}^2$
Modulus of elasticity	$E = 210000 \text{ N/mm}^2$



Partial factors - Section 6.1

Resistance of cross-sections	$\gamma_{M0} = 1.00$
Resistance of members to instability	$\gamma_{M1} = 1.00$
Resistance of tensile members to fracture	$\gamma_{M2} = 1.10$

Lateral restraint

Span 1 has full lateral restraint

Effective length factors

Effective length factor in major axis	$K_y = 1.000$
Effective length factor in minor axis	$K_z = 1.000$
Effective length factor for torsion	$K_{LT,A} = 1.000$
	$K_{LT,B} = 1.000$

Classification of cross sections - Section 5.5

$$\varepsilon = \sqrt{[235 \text{ N/mm}^2 / f_y]} = 0.92$$



Internal compression parts subject to bending - Table 5.2 (sheet 1 of 3)

Width of section

$$c = d = 123.6 \text{ mm}$$

$$c / t_w = 23.1 \times \epsilon \leq 72 \times \epsilon$$

Class 1

Outstand flanges - Table 5.2 (sheet 2 of 3)

Width of section

$$c = (b - t_w - 2 \times r) / 2 = 65.6 \text{ mm}$$

$$c / t_f = 10.4 \times \epsilon \leq 14 \times \epsilon$$

Class 3

Section is class 3

Check shear - Section 6.2.6

Height of web

$$h_w = h - 2 \times t_f = 138.8 \text{ mm}$$

Shear area factor

$$\eta = 1.000$$

$$h_w / t_w < 72 \times \epsilon / \eta$$

Shear buckling resistance can be ignored

Design shear force

$$V_{Ed} = \max(\text{abs}(V_{max}), \text{abs}(V_{min})) = 28 \text{ kN}$$

Shear area - cl 6.2.6(3)

$$A_v = \max(A - 2 \times b \times t_f + (t_w + 2 \times r) \times t_f, \eta \times h_w \times t_w) = 997 \text{ mm}^2$$

Design shear resistance - cl 6.2.6(2)

$$V_{pl,Rd} = A_v \times (f_y / \sqrt{3}) / \gamma_{M0} = 158.4 \text{ kN}$$

PASS - Design shear resistance exceeds design shear force

Check bending moment major (y-y) axis - Section 6.2.5

Design bending moment

$$M_{Ed} = \max(\text{abs}(M_{s1_max}), \text{abs}(M_{s1_min})) = 35.4 \text{ kNm}$$

Design bending resistance moment - eq 6.14

$$M_{c,Rd} = M_{el,Rd} = W_{el,y} \times f_y / \gamma_{M0} = 45.1 \text{ kNm}$$

PASS - Design bending resistance moment exceeds design bending moment

Check vertical deflection - Section 7.2.1

Consider deflection due to variable loads

Limiting deflection

$$\delta_{lim} = L_{s1} / 360 = 14 \text{ mm}$$

Maximum deflection span 1

$$\delta = \max(\text{abs}(\delta_{max}), \text{abs}(\delta_{min})) = 0 \text{ mm}$$

PASS - Maximum deflection does not exceed deflection limit