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# Development of land at former Wombwell High School Barnsley

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## Flood Risk Assessment

**Client:**

Premier Construction Northern  
51 Rimington Road  
Wombwell  
Barnsley  
S73 8DQ

**Prepared by:**

**joc consultants ltd**

Park Farm House  
Leathley Lane  
Leathley  
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LS21 2JU

## REVISION HISTORY

Revision	Date	Details
00	11 <sup>th</sup> January 2019	First issue

## APENDICES

- A: Location Plan
- B: Topographical survey plan
- C: Site Layout Plan
- D: Fluvial flood map
- E: Surface water flood map
- F: Reservoirs flood map
- G: REFH results
- H: Report of infiltration tests – Eastwood and Partners

## ABBREVIATIONS

AEP: Annual exceedance probability

AOD: Above Ordnance Datum

CCA: Climate change allowance

E: East

FEH: Flood Estimation Handbook

FRA: Flood risk assessment

NE: North east

PPG: Planning Practice Guidance

SE: South east

SFRA: Strategic Flood Risk Assessment

ReFH2: Revitalised Flood Hydrograph model, version 2

<b>SITE</b>	Land at former Wombwell High School, Lundhill Road, Wombwell, Barnsley, S73 0RA.
<b>PURPOSE OF THIS REPORT</b>	This site-specific flood risk assessment is required in connection with a planning application to Barnsley Metropolitan Borough Council for residential development of the site.
<b>SITE LOCATION AND DESCRIPTION</b>	See Location Plan in Appendix A.
<b>National Grid Reference</b>	440295E, 402435N approx
<b>Gross Site Area</b>	Approximately 6.76 ha
<b>Ground surface</b>	100% pervious surface.
<b>Topography</b>	Ground levels fall towards the northern apex of the site in the range 74.7m to 50.03m AOD. See topographical survey plan in Appendix B.
<b>Geology</b>	<u>Superficial</u> : None recorded. <u>Bedrock</u> : Oaks Rock - Sandstone.
<b>Watercourses</b>	None within the vicinity of the site. <b>The site is not within 20m of a Main River.</b>
<b>Reservoirs and Canals</b>	No reservoirs within the vicinity of the site. Elsescar Canal (disused) passes around the SE, E and NE sides of the site and is approximately 220m from the site at its nearest point.
<b>Existing site drainage</b>	There is no evidence of an existing drainage system on the topographical survey plan.
<b>Existing sewers</b>	It is not known whether there are any sewers crossing the site.
<b>THE DEVELOPMENT</b>	A development of 229 dwellings is proposed as shown on the Site Layout Plan in Appendix C. Access to the site will be off Lundhill Road, as shown on the site layout plan.

<b>VULNERABILITY CLASSIFICATION</b>	The development is classified as <b>'More Vulnerable'</b> , in accordance with Table 2 of the Planning Practice Guidance for Flood Risk and Coastal Change, paragraph 066.
<b>FLOOD ZONE</b>	Flood zone 1, (see Appendix D). <u>Reference:</u> Flood Map for Planning.
<b>REQUIREMENT TO CONSULT THE ENVIRONMENT AGENCY</b>	Not required when the development is in flood zone 1 and not within 20m of a main river or in a critical drainage area. <u>Reference:</u> Environment Agency Standing Advice.
<b>THE SEQUENTIAL TEST</b>	The Sequential Test is not required as the development is in Flood Zone 1.
<b>REQUIREMENT FOR THE EXCEPTION TEST</b>	Not required as the development is in Flood Zone 1. <u>Reference:</u> Planning Practice Guidance for Flood Risk and Coastal Change, paragraph 067.
<b>HISTORY OF FLOODING</b>	There is no available evidence of historic or potential flooding of the site.
<b>FLUVIAL FLOODING</b>	
<b>Functional floodplain</b>	The site is not in the functional floodplain.
<b>Annual probability of fluvial flooding</b>	Less than 0.1%.
<b>Flood defences</b>	None
<b>Loss of floodplain storage</b>	None
<b>Obstruction to overland flow routes</b>	None
<b>Flood warning area</b>	The site is not in a Flood Warning Area

## **SURFACE WATER FLOODING**

### **Risk of surface water flooding**

The Updated Surface Water Flood Map indicates a very low risk with no depths indicated.

See Appendix E.

### **Critical Drainage Areas**

The site is not in a critical drainage area.

## **GROUNDWATER FLOODING**

Groundwater flooding occurs when the water table rises above the ground surface or enters basements. It is typically associated with highly permeable rock such as chalk and highly fissured limestone. These geological conditions are not present at the site and the risk of this type of flooding at the site is therefore assessed to be very low.

## **SEWER FLOODING**

The site in its existing condition is not at risk from sewer flooding. Following development, sewer flooding could occur if the capacity of the sewers is exceeded, but the risk of such flooding is assessed to be low.

## **FLOODING FROM RESERVOIRS AND CANALS**

The site is not in an area at risk of flooding from reservoirs or canals.

See Appendix F.

## **EFFECT OF THE DEVELOPMENT ON FLOOD RISK**

### **Fluvial and tidal flood risk**

No effect

### **Surface water flood risk**

The effect of the development on surface water runoff rates and volumes has been assessed using FEH Point Data and the ReFH2 model. A summary of the results is provided in Appendix G.

The results show that the development, which is assumed for the purposes of this FRA to convert 50% of the site to impervious area, will potentially increase runoff rates and volumes by an average of 53% and 30% respectively.

### **Groundwater flood risk**

No effect

**Sewer flooding risk**

No effect

**EFFECT OF CLIMATE CHANGE**

Climate change must be considered over the expected lifetime of the development which, for residential development is defined to be 100 years in paragraph 026 of the Planning Practice Guidance. Climate change must therefore be considered up to 2118.

Current guidance on the application of climate change allowances was issued in February 2016 and updated on 3<sup>rd</sup> February 2017. The guidance provides the anticipated changes to peak river flow and rainfall intensity for different scenarios of carbon dioxide emissions over future epochs up to 2115.

The effects of climate change on peak river flow will not affect the flood zone designation throughout the lifetime of the development as the site is not at risk from fluvial flooding.

The current guidance requires the Central and Upper End allowances to be used when assessing the effects of increases to peak rainfall intensities. The allowances apply across the whole of England and in the period 2070 to 2115 are:

- Central allowance: 20%
- Upper end allowance: 40%

The effects of these climate change allowances are shown in the summary of the ReFH2 results in Appendix G and the detailed drainage design must take into account the range of climate change effects on surface water runoff.

**FLOOD RISK MANAGEMENT**

**Fluvial flood risk**

No recommendations

**Surface water flood risk**

The effect of the development on surface water flood risk can be mitigated by the application of sustainable drainage principles in the detailed drainage design of the drainage system.

*Peak flow control*

The underlying geology of the site suggests that infiltration drainage could be feasible. Infiltration tests were carried by Eastwood and Partners in December 2018 and their report is provided in Appendix H.

The report concludes that infiltration drainage will be feasible in the areas of sand and gravel, but where reworked clay is present the infiltration rates were poor.

*Attenuation storage*

Attenuation storage will be required to accommodate the excess runoff volume from the critical duration event. The form and capacity of this storage will be determined in the detailed design of the drainage system for the development.

As a preliminary estimate, the required storage capacity, should surface water be discharged to a sewer, is estimated to be:

- 1% AEP with 20% CCA: 2,072m<sup>3</sup>
- 1% AEP with 40% CCA: 2,527m<sup>3</sup>

The actual storage capacity will need to be verified in the detailed drainage design.

In the event that infiltration drainage is proposed, the storage capacity will depend on the infiltration rate determined in field tests.

**Groundwater flood risk**

No recommendations.

**Sewer flooding risk**

No recommendations.

**Reservoir flood risk**

No recommendations.

## CONCLUSIONS

1. The development classification is **More Vulnerable**.
2. The site is in flood zone 1 where the annual probability of fluvial flooding is less than 0.1%.
3. There is no requirement for the Environment Agency to be consulted on this development.
4. There is no requirement for the Sequential Test or the Exception Test as the proposed development is in Flood Zone 1.
5. There is no evidence of historic flooding at the site.
6. The risk of surface water flooding is very low.
7. The risk of groundwater flooding is assessed to be low.
8. The risk of sewer flooding is assessed to be low.
9. The site is not in an area at risk of flooding from reservoirs or canals.
10. The development will increase peak surface water runoff rates by approximately 53% and peak surface water runoff volume by approximately 30%.  
  
The effect of the development can be mitigated by the application of sustainable drainage principles, limiting the runoff rate and providing attenuation storage for the excess runoff volume.
11. The geology underlying the site suggests that infiltration drainage could be feasible and infiltration tests have confirmed this in the areas where there is sand and gravel.

## **RECOMMENDATIONS**

1. It is recommended that a detailed drainage design is prepared and submitted to Barnsley MDC and Yorkshire Water for approval, prior to construction.

## **USE OF REPORT**

This report is prepared specifically for Premier Construction Northern for the purpose of the aforementioned planning application and the report may not be used for any other purpose and it may not be assigned to any third party without our written permission.

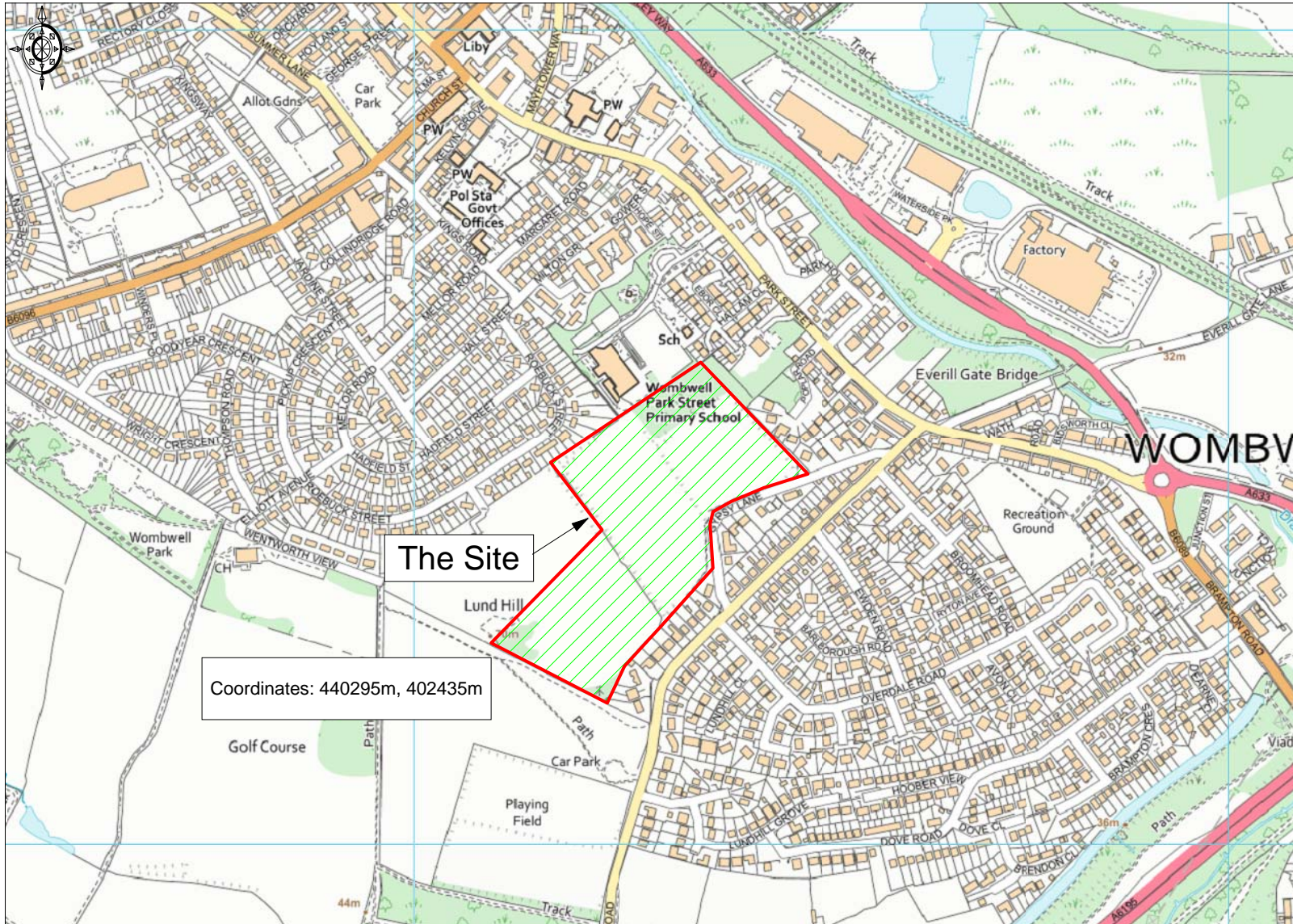
## **DISCLAIMER**

This flood risk assessment is based on data available at the time of its preparation and JOC Consultants Ltd accepts no liability for the consequences of any changes to or re-assessment of this data in the future.

## **APPENDIX A**

### **Location Plan**

Former Wombwell High School Site, off Lundhill Road, Wombwell, S70 0RA



Ordnance Survey © Crown Copyright 2019. All rights reserved. Licence number 100022432. Plotted Scale - 1:7500

Figure 1: Location Plan

## **APPENDIX B**

### **Topographical Survey Plan**



## **APPENDIX C**

### **Site Layout Plan**

Reference	Code	Floor Area (sqm)	Beds	Storeys	Total	Total Sqft	% of Mix
<b>Private</b>							
Type L	624	2	1	2	1248	13.6	1.0
Bungalow PB	832	3	1	3	2496	27.3	2.1
Type F	839	3	2	31	26009	286.1	22.7
Type H	919	3	2	15	13785	149.7	11.7
Type S	978	3	2	28	27384	296.1	23.5
Type T	1055	3	2	10	10550	114.4	9.0
Type C	1000	3	2	4	4000	43.2	3.4
Type G	1100	3	2.5	20	22000	239.1	18.8
Type D	1215	4	2	28	34020	367.8	28.8
Type J	1200	4	2.5	38	45600	493.7	38.5
Type A	1296	4	2	14	18144	196.7	15.3
Type E	1420	4	2	13	18460	200.0	15.6
<b>Sub-Total</b>				<b>206</b>	<b>223696</b>	<b>2434.1</b>	<b>100.0</b>
<b>Affordable</b>							
Type L	624	2	1	4	2496	27.3	2.1
Type B	685	2	2	19	13015	141.1	10.9
<b>Sub-Total</b>				<b>23</b>	<b>15511</b>	<b>168.4</b>	<b>13.0</b>
<b>Grand Total</b>				<b>229</b>	<b>239207</b>	<b>2592.5</b>	<b>100.0</b>

	hectares	acres
Approx gross area	7.72	19.08
Gross developable area	7.39	18.26
POS required (15%)	1.11	2.74
POS provided	1.12	2.77
net developable area coverage	5.92	14.63
	39	16332

**Notes:**  
 This drawing design and concepts are copyright of STEN Architecture.  
 All Dimensions are to be verified on site before any work commences. If any discrepancies, errors or omissions are noted, these are to be report to STEN architecture immediately.  
 If any other drawings are reference within this layout, please refer to the specific detailed drawing for design, materials and specific working practices.

- PLANNING LAYOUT KEY:**
- Boundary treatments**
- Brick wall
  - Close boarded timber fence
  - Property division
  - Metal railings
  - Post & rail
  - 450 Knee rail
- General**
- Affordable plot
  - Bin collection point (bin collection day only)
  - Site boundary
  - Herringbone Block paving
  - Retained tree



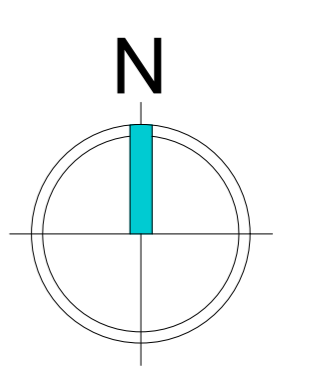
REV.	DESCRIPTION	BY	DATE

**STEN ARCHITECTURE**  
 Suite 4, Unit 1, Broomfield Park, Broomfield Avenue, Wombwell, West Yorkshire WF13 8BA, UK. Tel: 0113 259424. Web: www.sten-architecture.co.uk. Twitter: @STEN\_ARCH. Facebook: STENArchitecture. LinkedIn: Sten Architecture.

CLIENT: Premier group of companies  
 51 Rivington Road  
 Wombwell  
 Barnsley  
 S73 8DQ

SITE: Wombwell  
 TITLE: Planning Layout

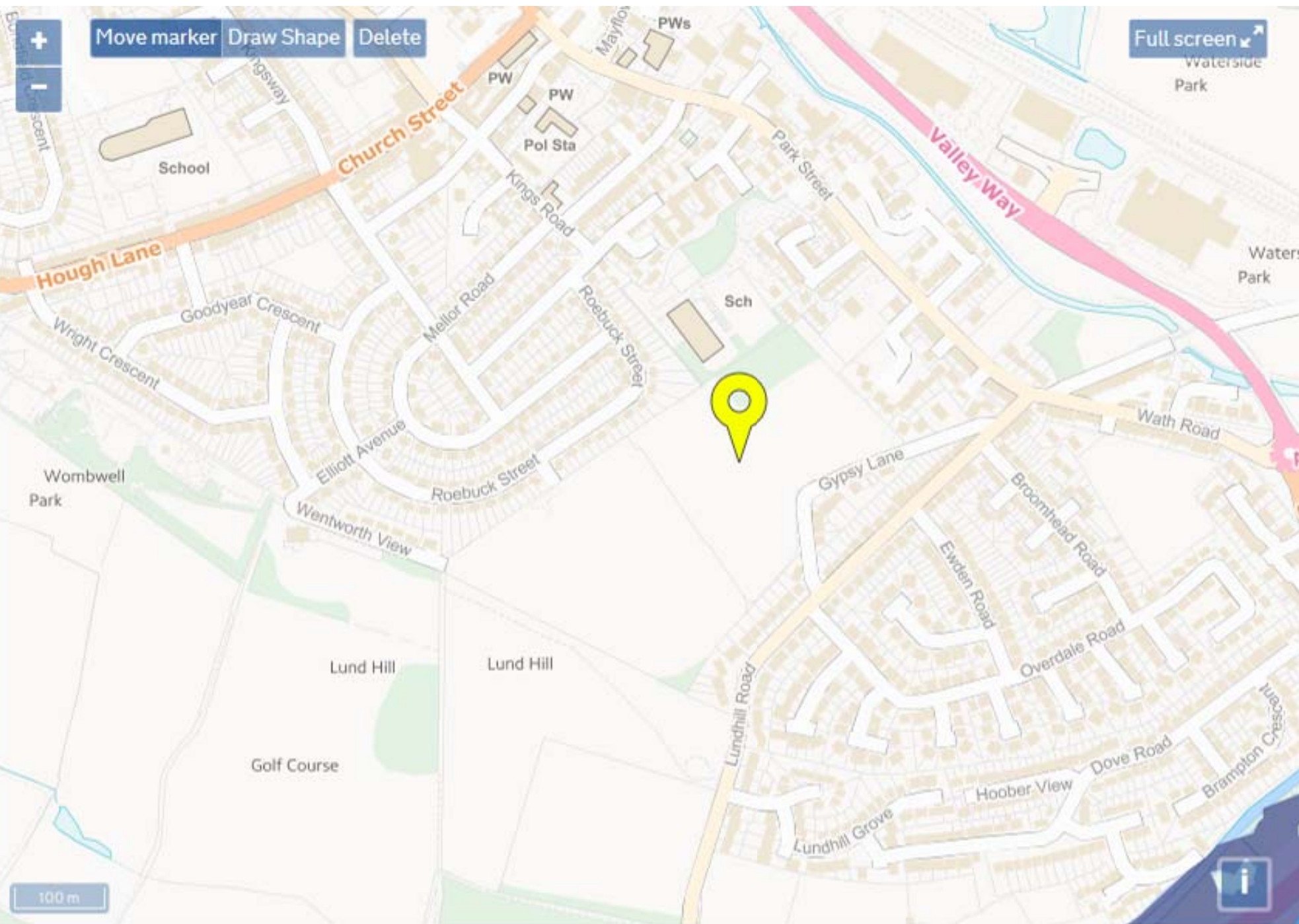
SCALE AT NO.	DATE	DRAWN	CHECKED
1:500	13.12.18	TS	--
PROJECT NO.	DRAWING NO.	REVISION	
1876	1876.01	--	



Scaled @ 1:500  
 0 10m 20m 50m

## **APPENDIX D**

### **Fluvial flood map**



Selected location



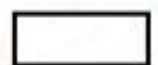
Flood zone 3



Areas benefiting from flood defences



Flood zone 2



Flood zone 1



Flood defence



Main river



Flood storage area

## **APPENDIX E**

### **Surface water flood map**



### Flood risk from rivers or the sea

- Extent of flooding
- Depth and flow estimates at monitoring stations



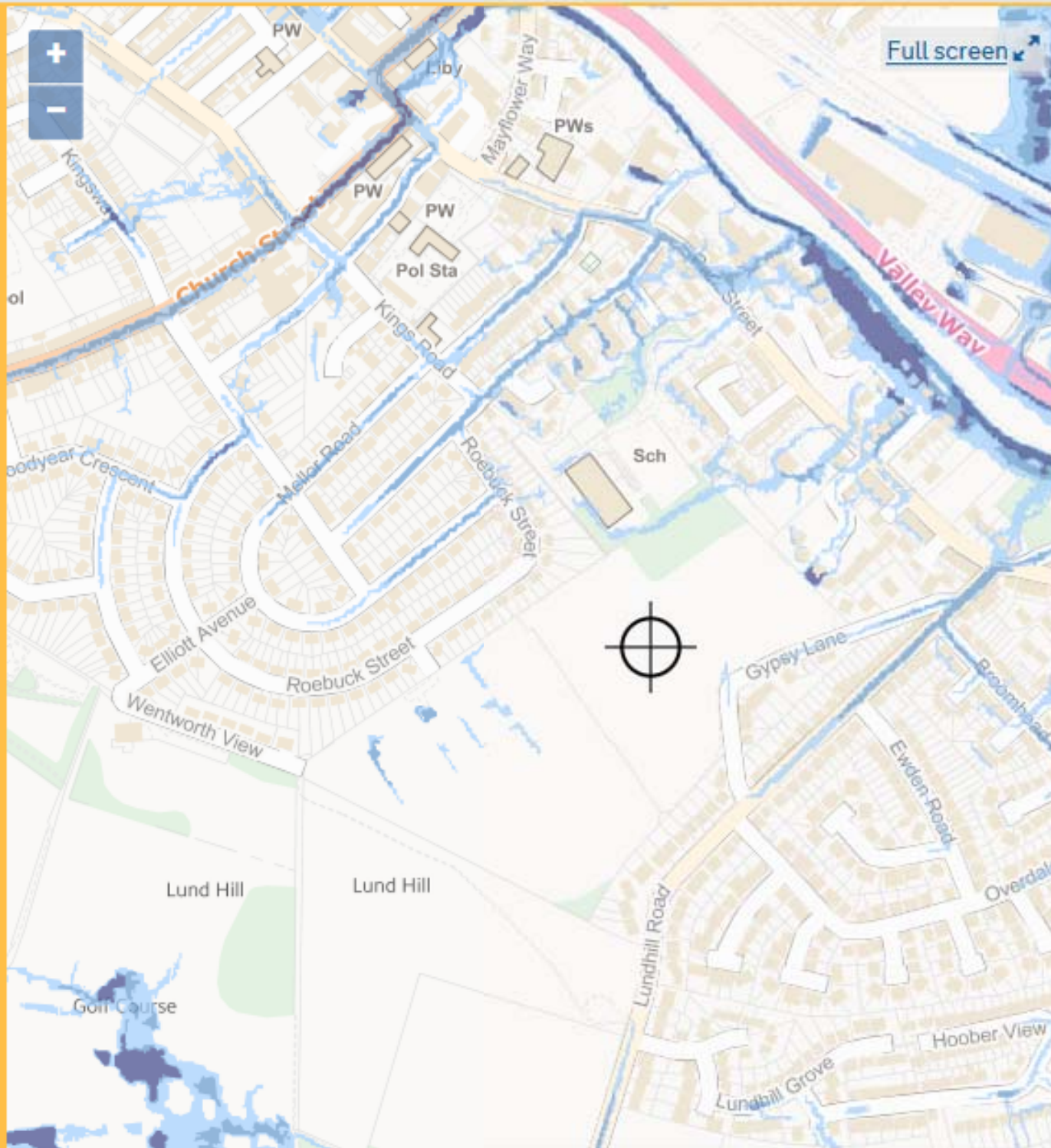
### Flood risk from surface water

- Extent of flooding
- High risk: depth
- High risk: velocity
- Medium risk: depth
- Medium risk: velocity
- Low risk: depth
- Low risk: velocity



### Flood risk from reservoirs

- Extent of flooding
- Flood depth



### Flood risk



High



Medium



Low



Very low



Location you selected

## **APPENDIX F**

### **Reservoirs flood map**



### Flood risk from rivers or the sea

- Extent of flooding
- Depth and flow estimates at monitoring stations



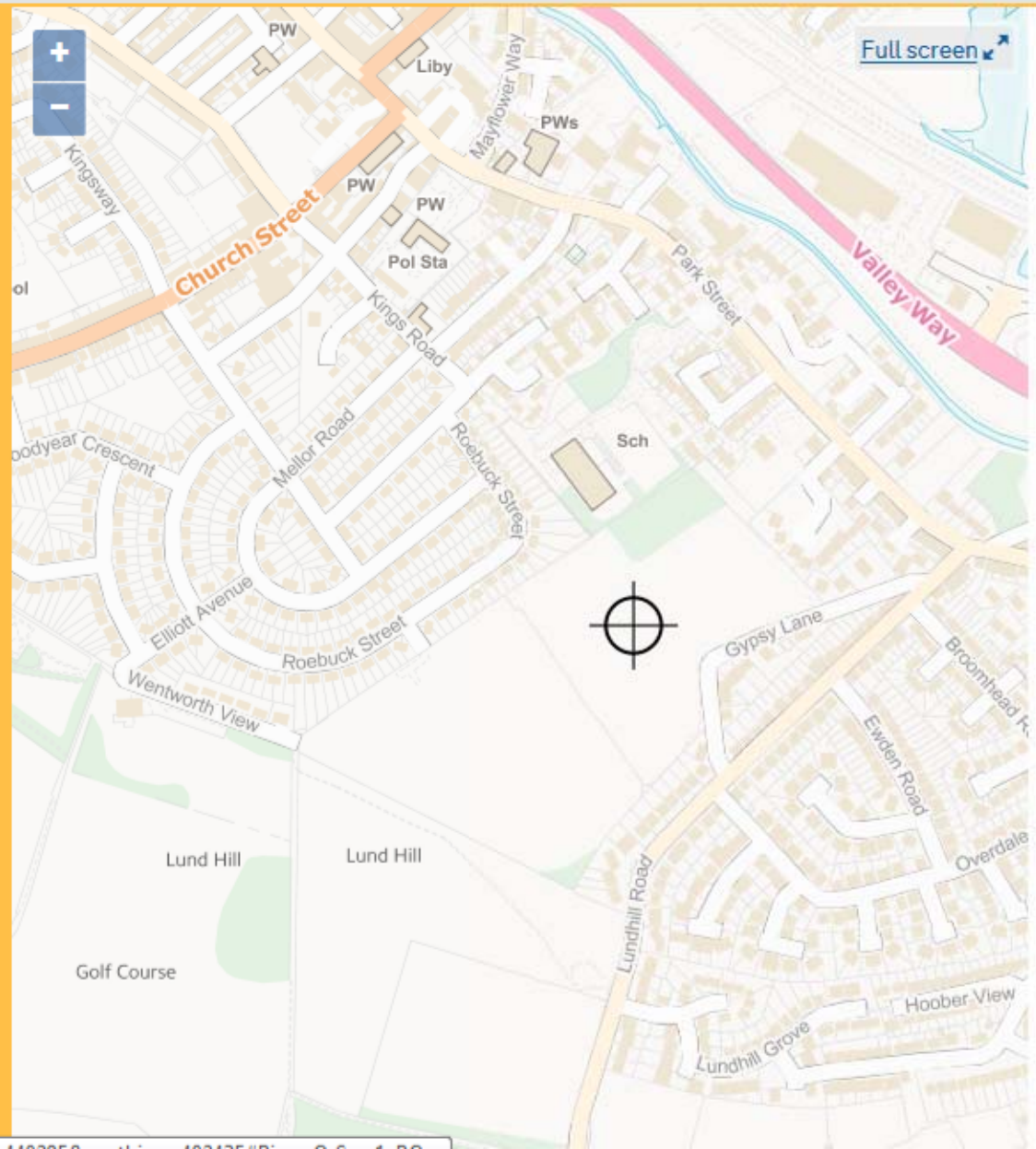
### Flood risk from surface water

- Extent of flooding
- High risk: depth
- High risk: velocity
- Medium risk: depth
- Medium risk: velocity
- Low risk: depth
- Low risk: velocity



### Flood risk from reservoirs

- Extent of flooding
- Flood depth



### Flood risk



Maximum extent of flooding



Location you selected

## **APPENDIX G**

### **REFH2 Results**

19/003: Wombwell High School Site

SUMMARY OF REFH RESULTS

Event AEP	Greenfield		Brownfield		Post development		% change	
	Peak Flow l/s	Volume m <sup>3</sup>	Peak Flow l/s	Volume m <sup>3</sup>	Peak Flow l/s	Volume m <sup>3</sup>	Peak Flow	Volume
100%	33.11	431.56			51.55	574.53	56%	33%
50%	37.59	496.38			58.57	658.80	56%	33%
3.3%	86.05	1,197.46			131.28	1,542.09	53%	29%
1%	119.25	1,678.73			178.28	2,122.81	50%	26%
						Average:	53%	30%
1% - 20% CCA					214.06	2568.77		
1% - 40% CCA					250.59	3023.35		
Estimate of attenuation storage required:					20% CCA	2072.39		
					40% CCA	2526.97		

# UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:04:58 AM by John  
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

## Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

### Site details

Checksum: 1DB7-59BB

Site name: Wombwell High School Site - Greenfield  
Easting: 440289  
Northing: 402467  
Country: England, Wales or Northern Ireland  
Catchment Area (km<sup>2</sup>): 0.07  
Using plot scale calculations: Yes  
Site description: Greenfield

## Model run: 1 year

### Summary of results

Rainfall - FEH 2013 (mm):	16.95	Total runoff (ML):	0.43	431.56 m <sup>3</sup>
Total Rainfall (mm):	10.61	Total flow (ML):	0.75	
Peak Rainfall (mm):	3.59	Peak flow (m <sup>3</sup> /s):	0.03	33.11 l/s

### Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

\* Indicates that the user locked the duration/timestep

#### Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

#### Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

#### Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

#### Baseflow model parameters

Name	Value	User-defined?
BF0 (m <sup>3</sup> /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

#### Urbanisation parameters

Name	Value	User-defined?
Urban area (km <sup>2</sup> )	0	No
Urbext 2000	0	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Sewered area (km <sup>2</sup> )	0.00	Yes
Sewer capacity (m <sup>3</sup> /s)	0.00	Yes

# UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:05:33 AM by John  
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

## Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

### Site details

Checksum: 1DB7-59BB

Site name: Wombwell High School Site - Greenfield  
Easting: 440289  
Northing: 402467  
Country: England, Wales or Northern Ireland  
Catchment Area (km<sup>2</sup>): 0.07  
Using plot scale calculations: Yes  
Site description: Greenfield

## Model run: 2 year

### Summary of results

Rainfall - FEH 2013 (mm):	19.40	Total runoff (ML):	0.50	496.38 m <sup>3</sup>
Total Rainfall (mm):	12.15	Total flow (ML):	0.86	
Peak Rainfall (mm):	4.10	Peak flow (m <sup>3</sup> /s):	0.04	37.59 l/s

### Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

\* Indicates that the user locked the duration/timestep

#### Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

#### Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

#### Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

#### Baseflow model parameters

Name	Value	User-defined?
BF0 (m <sup>3</sup> /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

#### Urbanisation parameters

Name	Value	User-defined?
Urban area (km <sup>2</sup> )	0	No
Urbext 2000	0	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Sewered area (km <sup>2</sup> )	0.00	Yes
Sewer capacity (m <sup>3</sup> /s)	0.00	Yes

# UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:05:51 AM by John  
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## Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

### Site details

Checksum: 1DB7-59BB

Site name: Wombwell High School Site - Greenfield  
Easting: 440289  
Northing: 402467  
Country: England, Wales or Northern Ireland  
Catchment Area (km<sup>2</sup>): 0.07  
Using plot scale calculations: Yes  
Site description: Greenfield

## Model run: 30 year

### Summary of results

Rainfall - FEH 2013 (mm):	44.58	Total runoff (ML):	1.20	1197.46 m <sup>3</sup>
Total Rainfall (mm):	27.91	Total flow (ML):	2.06	
Peak Rainfall (mm):	9.43	Peak flow (m <sup>3</sup> /s):	0.09	86.05 l/s

### Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

\* Indicates that the user locked the duration/timestep

#### Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

#### Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

#### Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

#### Baseflow model parameters

Name	Value	User-defined?
BF0 (m <sup>3</sup> /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

#### Urbanisation parameters

Name	Value	User-defined?
Urban area (km <sup>2</sup> )	0	No
Urbext 2000	0	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Sewered area (km <sup>2</sup> )	0.00	Yes
Sewer capacity (m <sup>3</sup> /s)	0.00	Yes

# UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:06:18 AM by John  
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

## Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

### Site details

Checksum: 1DB7-59BB

Site name: Wombwell High School Site - Greenfield  
Easting: 440289  
Northing: 402467  
Country: England, Wales or Northern Ireland  
Catchment Area (km<sup>2</sup>): 0.07  
Using plot scale calculations: Yes  
Site description: Greenfield

## Model run: 100 year

### Summary of results

Rainfall - FEH 2013 (mm):	60.65	Total runoff (ML):	1.68	1678.73 m <sup>3</sup>
Total Rainfall (mm):	37.97	Total flow (ML):	2.90	
Peak Rainfall (mm):	12.83	Peak flow (m <sup>3</sup> /s):	0.12	119.25 l/s

### Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

\* Indicates that the user locked the duration/timestep

#### Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

#### Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

#### Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

#### Baseflow model parameters

Name	Value	User-defined?
BF0 (m <sup>3</sup> /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

#### Urbanisation parameters

Name	Value	User-defined?
Urban area (km <sup>2</sup> )	0	No
Urbext 2000	0	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Sewered area (km <sup>2</sup> )	0.00	Yes
Sewer capacity (m <sup>3</sup> /s)	0.00	Yes

# UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:08:03 AM by John  
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

## Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

### Site details

Checksum: AFED-CF4C

Site name: Wombwell High School Site  
Easting: 440289  
Northing: 402467  
Country: England, Wales or Northern Ireland  
Catchment Area (km<sup>2</sup>): 0.07  
Using plot scale calculations: Yes  
Site description: Post development

## Model run: 1 year

### Summary of results

Rainfall - FEH 2013 (mm):	16.95	Total runoff (ML):	0.57	574.53 m <sup>3</sup>
Total Rainfall (mm):	10.61	Total flow (ML):	0.73	
Peak Rainfall (mm):	3.59	Peak flow (m <sup>3</sup> /s):	0.05	51.55 l/s

### Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

\* Indicates that the user locked the duration/timestep

#### Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

#### Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

#### Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

#### Baseflow model parameters

Name	Value	User-defined?
BF0 (m <sup>3</sup> /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

#### Urbanisation parameters

Name	Value	User-defined?
Urban area (km <sup>2</sup> )	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km <sup>2</sup> )	0.00	Yes
Sewer capacity (m <sup>3</sup> /s)	0.00	Yes

# UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:08:46 AM by John  
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

## Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

### Site details

Checksum: AFED-CF4C

Site name: Wombwell High School Site  
Easting: 440289  
Northing: 402467  
Country: England, Wales or Northern Ireland  
Catchment Area (km<sup>2</sup>): 0.07  
Using plot scale calculations: Yes  
Site description: Post development

## Model run: 2 year

### Summary of results

Rainfall - FEH 2013 (mm):	19.40	Total runoff (ML):	0.66	658.80 m <sup>3</sup>
Total Rainfall (mm):	12.15	Total flow (ML):	0.84	
Peak Rainfall (mm):	4.10	Peak flow (m <sup>3</sup> /s):	0.06	58.57 l/s

### Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

\* Indicates that the user locked the duration/timestep

#### Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

#### Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

#### Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

#### Baseflow model parameters

Name	Value	User-defined?
BF0 (m <sup>3</sup> /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

#### Urbanisation parameters

Name	Value	User-defined?
Urban area (km <sup>2</sup> )	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km <sup>2</sup> )	0.00	Yes
Sewer capacity (m <sup>3</sup> /s)	0.00	Yes

# UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:09:05 AM by John  
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

## Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

### Site details

Checksum: AFED-CF4C

Site name: Wombwell High School Site  
Easting: 440289  
Northing: 402467  
Country: England, Wales or Northern Ireland  
Catchment Area (km<sup>2</sup>): 0.07  
Using plot scale calculations: Yes  
Site description: Post development

## Model run: 30 year

### Summary of results

Rainfall - FEH 2013 (mm):	44.58	Total runoff (ML):	1.54	1542.09 m <sup>3</sup>
Total Rainfall (mm):	27.91	Total flow (ML):	1.97	
Peak Rainfall (mm):	9.43	Peak flow (m <sup>3</sup> /s):	0.13	131.28 l/s

### Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

\* Indicates that the user locked the duration/timestep

#### Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

#### Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

#### Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

#### Baseflow model parameters

Name	Value	User-defined?
BF0 (m <sup>3</sup> /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

#### Urbanisation parameters

Name	Value	User-defined?
Urban area (km <sup>2</sup> )	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km <sup>2</sup> )	0.00	Yes
Sewer capacity (m <sup>3</sup> /s)	0.00	Yes

# UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:09:31 AM by John  
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

## Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

### Site details

Checksum: AFED-CF4C

Site name: Wombwell High School Site  
Easting: 440289  
Northing: 402467  
Country: England, Wales or Northern Ireland  
Catchment Area (km<sup>2</sup>): 0.07  
Using plot scale calculations: Yes  
Site description: Post development

## Model run: 100 year

### Summary of results

Rainfall - FEH 2013 (mm):	60.65	Total runoff (ML):	2.12	2122.81 m <sup>3</sup>
Total Rainfall (mm):	37.97	Total flow (ML):	2.73	
Peak Rainfall (mm):	12.83	Peak flow (m <sup>3</sup> /s):	0.18	178.28 l/s

### Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

\* Indicates that the user locked the duration/timestep

#### Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

#### Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

#### Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

#### Baseflow model parameters

Name	Value	User-defined?
BF0 (m <sup>3</sup> /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

#### Urbanisation parameters

Name	Value	User-defined?
Urban area (km <sup>2</sup> )	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km <sup>2</sup> )	0.00	Yes
Sewer capacity (m <sup>3</sup> /s)	0.00	Yes

# UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:24:45 AM by John  
 Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

## Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

### Site details

Checksum: 1167-CB3B

Site name: Wombwell High School Site

Easting: 440289

Northing: 402467

Country: England, Wales or Northern Ireland

Catchment Area (km<sup>2</sup>): 0.07

Using plot scale calculations: Yes

Site description: Post development: 1% AEP & 20% CCA

## Model run: 200 year

### Summary of results

Rainfall - FEH 2013 (mm):	72.75	Total runoff (ML):	2.57	2568.77 m <sup>3</sup>
Total Rainfall (mm):	45.55	Total flow (ML):	3.31	
Peak Rainfall (mm):	15.39	Peak flow (m <sup>3</sup> /s):	0.21	214.06 l/s

### Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

\* Indicates that the user locked the duration/timestep

#### Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

#### Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

#### Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

#### Baseflow model parameters

Name	Value	User-defined?
BF0 (m <sup>3</sup> /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

#### Urbanisation parameters

Name	Value	User-defined?
Urban area (km <sup>2</sup> )	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km <sup>2</sup> )	0.00	Yes
Sewer capacity (m <sup>3</sup> /s)	0.00	Yes

# UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:25:12 AM by John  
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

## Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

### Site details

Checksum: 1167-CB3B

Site name: Wombwell High School Site

Easting: 440289

Northing: 402467

Country: England, Wales or Northern Ireland

Catchment Area (km<sup>2</sup>): 0.07

Using plot scale calculations: Yes

Site description: Post development: 1% AEP & 40% CCA

## Model run: 367 year

### Summary of results

Rainfall - FEH 2013 (mm):	84.88	Total runoff (ML):	3.02	3023.35 m <sup>3</sup>
Total Rainfall (mm):	53.14	Total flow (ML):	3.92	
Peak Rainfall (mm):	17.95	Peak flow (m <sup>3</sup> /s):	0.25	250.59 l/s

### Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

\* Indicates that the user locked the duration/timestep

#### Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

#### Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

#### Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

#### Baseflow model parameters

Name	Value	User-defined?
BF0 (m <sup>3</sup> /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

#### Urbanisation parameters

Name	Value	User-defined?
Urban area (km <sup>2</sup> )	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km <sup>2</sup> )	0.00	Yes
Sewer capacity (m <sup>3</sup> /s)	0.00	Yes

## **APPENDIX H**

### **Report of infiltration tests**

Eastwood and Partners report dated 27<sup>th</sup> December 2018

Mr M Platts  
Premier Group  
51 Rimington Road  
Wombwell  
Barnsley  
S73 8DQ

PR/AJK/SAE/43497-001

27 December 2018

Dear Martyn,

### **Wombwell High School**

We are writing to report the findings of the infiltration testing undertaken on the above site on 17 and 18 December 2018.

The site comprises a former school, now demolished, and associated playing fields. The site is split into three terraces, with the upper terrace and former school present in the west of the site, and the lowest terrace present in the east of the site. A difference in level of approximately 5 m bgl is present between each terrace.

### **Site Works**

Nine soakaway pits were excavated across the site, to depths of between 1.2 m and 2.3 m below ground level (bgl).

Water was then pumped in to each pit to a depth of at least 500 mm, and the change in water level was monitored at regular intervals over at least a three hour period, or until the water had drained from each pit, whichever came first. Between one and three infiltration tests were undertaken in each pit.

Two trial pits were additionally excavated to 2.4 m and 3.4 m bgl, in order to assess the depth of fill in the east of the uppermost terrace.

The locations of the soakaway and trial pits are shown on the Exploratory Hole Location Plan, drawing number 43497/001/A, which is appended to this report.

---

Also at: - Centaur House, Ancells Business Park, Ancells Rd, Fleet GU51 2UJ Tel: 01252 360580 Fax: 01252 360581

**Directors:** P Richardson BSc, CEng, MICE, MIStructE S D Preston BEng, CEng, FICE, FIStructE N J Baines BSc, CEng, MICE, MCIWEM  
S R Ellis BEng, CEng, MIStructE, MICE K R Pursall BEng, CEng, MIStructE

C A Topliss BSc, CEng, CSci, CGeol, SiLC, MICE, FGS S J English BEng, CEng, MIStructE A R Priest BEng

**Senior Associates:** K Newsome BSc, CEng, MICE, MIStructE S J Mitchell BSc, MSc, CEng, MEI, MCIBSE, MASHRAE A Allison BEng

M Young MA, CEng, MICE, MIStructE C A Wood BSc, CEng, MIStructE, MICE

**Associates:** K Edwards MSci, FGS A J Kerslake BEng A G Marshall BEng, CEng, MIStructE C Hodge EngTech, MICE P A Harrison BEng, CEng, MIStructE  
M P Chappell BEng, IEng, AMIStructE M Dyson BSc, CEng, MIStructE

## Ground Conditions

Historically, a cut and fill earthworks exercise has occurred on the site in order to create three flat terraces for the former school playing fields. Generally the surrounding land slopes from the west down to the east.

Topsoil comprising clayey sand, and occasionally sandy clay, was encountered in the excavations across the site to depths of between 0.3 m and 0.5 m bgl. This was underlain by clayey sand and gravel in SA3, SA6 and SA7, encountered to the base of the pit in SA3 and underlain by weak to medium strong sandstone at 1.1 m and 0.9 m bgl respectively in SA6 and SA7.

In the remainder of exploratory holes, made ground comprising sandy gravelly reworked clay, with occasional to frequent cobbles of sandstone with depth was encountered, with the depth of made ground increasing towards the east. This was underlain by natural sand and gravel from 0.6 m bgl in SA1 and SA4, and from 1.4 m bgl in SA7, and by weak to medium strong sandstone from depths of between 1.1 m and 2.25 m bgl in SA2, SA8, SA9, TP1 and TP2. Pits excavated in the west of each terrace generally recorded sandstone bedrock at shallower depth than those in the east of each terrace.

The trial pit and soakaway logs are appended to this report.

## Infiltration Results

The results and calculation of Infiltration Results are appended to this report, and are summarised in the table below:

Soakaway	Test Material	BRE365 Soil Infiltration Rate (x10-6) m/s	Average Infiltration Rate
SA1 Test 1	Reworked clay over sand and gravel	34	31
SA1 Test 2		69	56
SA1 Test 3		47	57
SA2	Reworked clay over sandstone at base	0	0
SA3 Test 1	Sand and gravel	360	580
SA3 Test 2		240	360
SA3 Test 3		310	430
SA4 Test 1	Reworked clay over sand and gravel	21	34
SA4 Test 2		25	40
SA5 Test 1	Reworked clay over sand and gravel	45	66
SA5 Test 2		18	33
SA6 Test 1	Sand and gravel over sandstone	220	310
SA6 Test 2		120	180
SA6 Test 3		120	160

SA7 Test 1	Gravel over sandstone	33	39
SA7 Test 2		17	25
SA8	Reworked clay over sandstone	-	2.5
SA9 Test 1	Reworked clay over sandstone	98	98
SA9 Test 2		64	76
SA9 Test 3		61	79

**Conclusion**

Soakaways excavated within sand and gravel generally performed the best, with those soakaways whose pit walls generally comprised reworked clay performing the worst overall.

Therefore it is recommended soakaways be constructed within the sand and gravel generally found to the west of each terrace, and avoid the made ground, found to extend to significant depth towards the east of each terrace.

We trust that this meets with your approval, however if you have any comments or queries please do not hesitate to contact us.

Yours sincerely






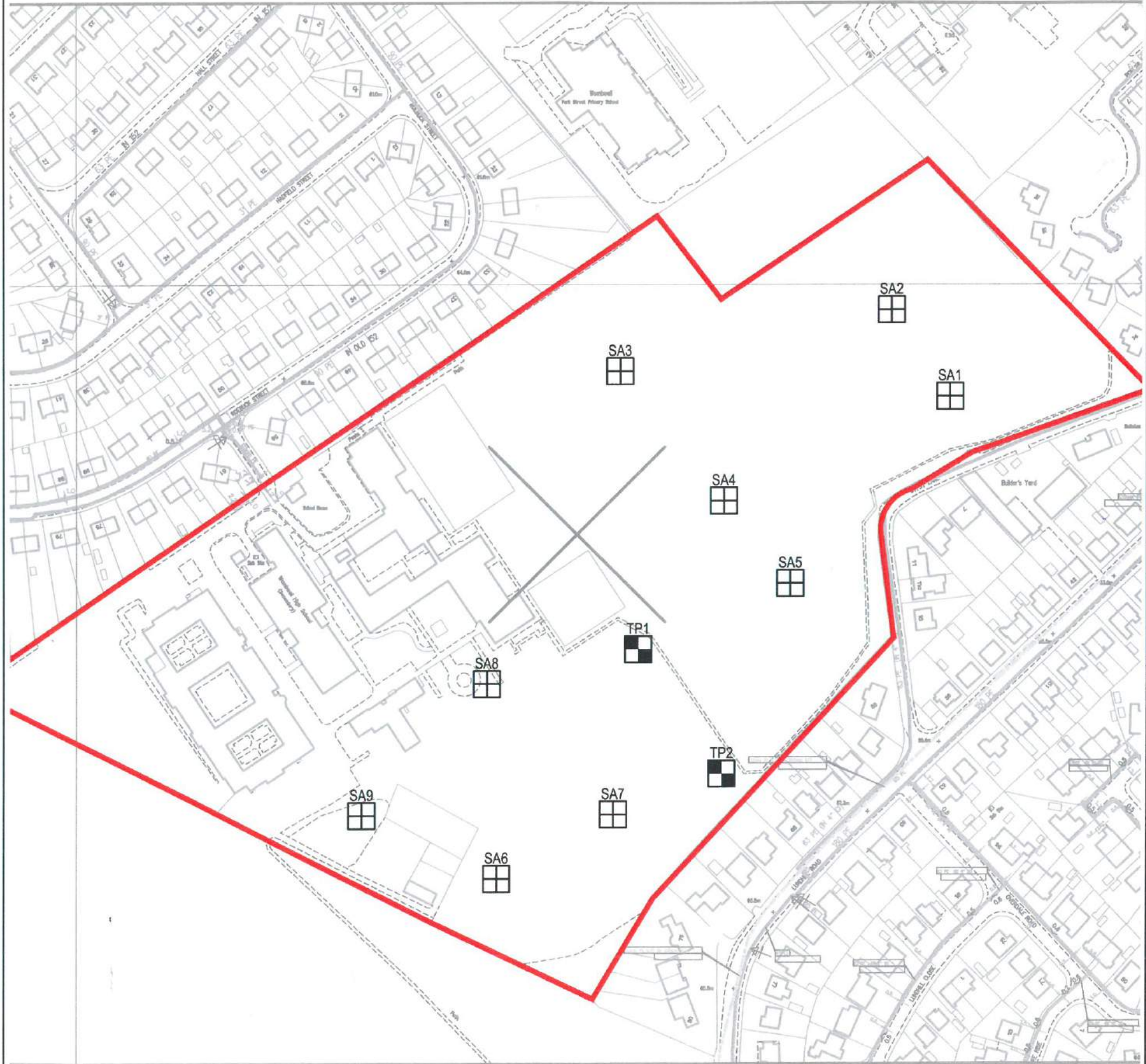
**Andrew Kerlake**  
Associate

- Enc. Exploratory Hole Plan
- Infiltration Results - SA1 to SA9
- Trial Pit and Soakaway Logs

INFORMATION WITHIN THIS DRAWING IS NOT NECESSARILY PRODUCED TO SCALE.  
ALWAYS USE FIGURED DIMENSIONS AND CO-ORDINATES - IF IN DOUBT, ASK.

**KEY:**

-  Approximate location of trial pits excavated by Eastwood and Partners on 18.12.18.
-  Approximate location of soakaway excavated by Eastwood and Partners between 17.12.18 and 18.12.18.
-  Site Boundary



A	First Issue.			
REV	DESCRIPTION	SIG	CHK	DATE

**PREMIER CONSTRUCTION  
NORTHERN LTD**

**WOMBWELL HIGH SCHOOL, GYPSY  
LANE, WOMBWELL**

**EXPLORATORY HOLE LOCATION PLAN**

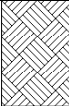

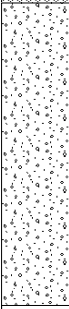
**Eastwood & Partners**   
CONSULTING ENGINEERS

St. Andrew's House  
23 Kingfield Road  
Sheffield S11 9AS  
Tel 0114 255 4554 Fax 0114 255 4330  
mail@eastwoodandpartners.com www.eastwoodandpartners.com

SCALE WHEN PLOTTED AT A3 1:2000			DRAWING STATUS <b>INFORMATION</b>	
DRAWN	CHECKED	DATE	DRAWING NUMBER	REV
TC	?	19.12.18	43497/001	A

This plan shows those pipes owned by Cadent Gas Ltd in their role as a

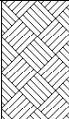
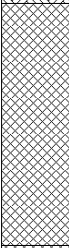
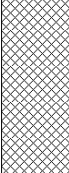
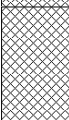

Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 2.50m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.60m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.35			TOPSOIL: Grass over dark brown sandy CLAY.
			0.60			MADE GROUND: Light brown /orange brown sandy reworked CLAY.
			1.60			Brown Clayey SAND and GRAVEL with occasional to frequent cobbles. Gravel is fine to coarse angular to sub-angular of sandstone.
						Trialpit Complete at 1.600m

Remarks:

Stability:

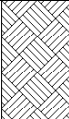
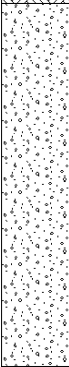
Project Name Wombwell High School		Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:			Dimensions: 2.90m	Scale 1:25
Client: Premier Construction Northern Ltd.			Depth: 2.25m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.40			TOPSOIL: Gras cover dark brown clayey SAND.
			1.20			MADE GROUND: Firm brown sandy reworked CLAY.
			1.80			MADE GROUND: Stiff to friable brown mottled grey sandy gravelly reworked CLAY with occasional cobbles. Gravel is medium to coarse angular to sub-angular of sandstone.
			2.20			MADE GROUND: Grey brown friable sandyreworked CLAY.
			2.25			Strong brown SANDSTONE. Trialpit Complete at 2.250m

Remarks:

Stability:



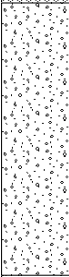
Project Name Wombwell High School		Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:			Dimensions: 2.90m	Scale 1:25
Client: Premier Construction Northern Ltd.			Depth: 1.60m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.40			TOPSOIL: Grass over dark brown clayey SAND.
			1.60			Orange brown clayey SAND and GRAVEL. Gravel is medium to coarse angular to sub-angular of sandstone. Occasional becoming frequent cobbles with depth.
						Trialpit Complete at 1.600m

Remarks:

Stability:


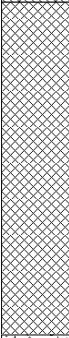
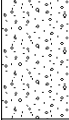
Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 3.10m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.50m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.30			TOPSOIL: Grass over dark brown clayey SAND.
			0.60			MADE GROUND: Brown very sandy reworked CLAY.
			1.50			Orange brown clayey SAND and GRAVEL. Gravel is fine to coarse subangular of sandstone. Occasional becoming frequent cobbles from 0.9 m bgl.
						Trialpit Complete at 1.500m

Remarks:

Stability:


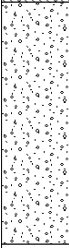

Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 2.80m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.80m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.30			TOPSOIL: Grass over dark brown clayey SAND.
			1.40			MADE GROUND: Brown sandy gravelly reworked CLAY with occasional cobbles. Gravel is fine to coarse sub-angular of sandstone.
			1.80			Brown slightly clayey SAND and GRAVEL. Gravel is fine to coarse sub-angular of sandstone, with occasional cobbles.
Trialpit Complete at 1.800m						

Remarks:

Stability:

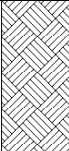
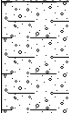
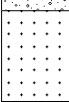
Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:	Dimensions: 3.00m Depth: 1.30m		Scale 1:25
Client: Premier Construction Northern Ltd.			Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.30			TOPSOIL: Grass over dark brown clayey SAND.
			1.10			Yellow/orange brown slightly clayey SAND and GRAVEL. Gravel is fine to coarse angular to subangular of sandstone. Frequent cobbles with depth.
			1.30			Weak to medium strong yellow brown SANDSTONE recovered as cobbles and gravel.
Trialpit Complete at 1.300m						

Remarks:

Stability:

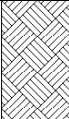

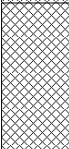

Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 3.10m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.20m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
						TOPSOIL: Grass over dark brown clayey SAND.
			0.50			Orange brown slightly clayey sandy GRAVEL. Gravel is fine to coarse angular to sub-angular of sandstone, with frequent cobbles with depth.
			0.90			Medium strong SANDSTONE recovered as sand gravel, with frequent cobbles.
			1.20			Trialpit Complete at 1.200m

Remarks:

Stability:

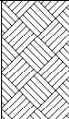

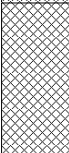

Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 3.20m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.30m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.40			TOPSOIL: Grass over dark brown clayey SAND.
			0.60			MADE GROUND: Brown sandy gravelly reworked CLAY. Gravel is fine to medium sub-angular of sandstone.
			1.10			POSSIBLE MADE GROUND: Yellow/orange brown sandy very gravelly CLAY. Gravel is fine to medium sub-angular of sandstone.
			1.30			Extremely weak to weak grey brown SANDSTONE, recovered as tabular gravel.
Trialpit Complete at 1.300m						

Remarks:

Stability:

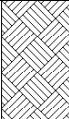
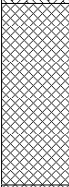

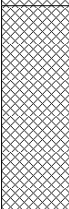
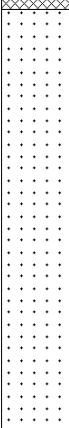
Project Name Wombwell High School		Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:			Dimensions: 3.20m	Scale 1:25
Client: Premier Construction Northern Ltd.			Depth: 1.25m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.40			TOPSOIL: Grass over dark brown clayey SAND.
			0.60			MADE GROUND: Brown sandy gravelly reworked CLAY. Gravel is fine to medium sub-angular of sandstone.
			1.10			POSSIBLE MADE GROUND: Yellowish brown sandy gravelly CLAY. Gravel is fine to coarse subangular of sandstone.
			1.25			Weak to medium strong yellow brown SANDSTONE, recovered as tabular gravel and cobbles.
Trialpit Complete at 1.250m						

Remarks:

Stability:


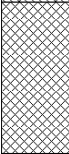
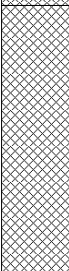

Project Name Wombwell High School		Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: <span style="float: right;">m</span>		Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 3.40m		Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.40			TOPSOIL: Dark Brown clayey SAND.
			1.00			MADE GROUND: Brown Sandy gravelly reworked CLAY with occasional cobbles. Gravel is fine to coarse sub-angular of SANDSTONE.
			1.30			MADE GROUND: Brown sclayey gravelly SAND. Gravel is fine to coarse sub-angular of SANDSTONE with occasional cobbles.
			2.00			MADE GROUND: Brown sandy gravelly reworked CLAY with occasional cobbles. Gravel is fine to coarse sub-angular of SANDSTONE.
			3.40			Extremely weak to weak grey brown SANDSTONE recovered as sand, gravel and occasional cobbles. Cobble content increases with depth.
						Trialpit Complete at 3.400m

Remarks:

Stability:

Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: <span style="float: right;">m</span>	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 2.40m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.30			TOPSOIL: Dark brown clayey SAND.
			0.80			MADE GROUND: Brown sandy gravelly reworked CLAY. Gravel is fine to coarse sub-angular of SANDSTONE.
			1.20			MADE GROUND: Brown sandy gravelly reworked CLAY. Gravel is fine to coarse sub-angular of SANDSTONE.
			2.10			MADE GROUND: Brown sandy gravelly reworked CLAY. Gravel is sub-angular of SANDSTONE.
			2.40			Medium strong brown SANDSTONE recovered as sand, gravel and cobbles.
						Trialpit Complete at 2.400m

Remarks:

Stability:



<b>PROJECT:</b>	<b>Wombwell High School</b>	<b>Job No.</b> 43497	<b>Date</b> 19.12.18
<b>SUBJECT:</b>	<b>Infiltration Test Results and Calculation of Infiltration Rates</b>	<b>Prepared</b> JA/SAE	<b>Checked</b> DN

**Test No. SA1 - Test 1**

**Soil Infiltration Rate in Accordance with BR365**

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

$V_{p75-25}$

Initial parameters

Depth to water = **1040 mm**      Average water depth: **280 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **560 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **600 mm**      Time interval: **140 min**

End time = **140 min**

Effective Storage Volume of Water in the Trial Pit = **0.75 m<sup>3</sup>**  
 75% Effective Depth = **1225 mm** from ground level  
 25% Effective Depth = **1475 mm** from ground level  
 Time at 75% Effective Depth = **4 minutes**  
 Time at 25% Effective Depth = **64 minutes**

= **0.38 m<sup>3</sup>**

= **3.05 m<sup>2</sup>**

= **3600 sec**

= **3.4E-05 m/sec**

Average Soakaway Rate = **1.0E-04 m<sup>3</sup>/sec**

Average soakaway area = **3.24 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$  **Soil Infiltration Rate = 3.4E-05 m/sec**  
Average Infiltration Rate = 3.1E-05 m/sec

$t_{p75-25}$



<b>PROJECT:</b>	<b>Wombwell High School</b>	<b>Job No.</b> 43497	<b>Date</b> 19.12.18
<b>SUBJECT:</b>	<b>Infiltration Test Results and Calculation of Infiltration Rates</b>	<b>Prepared</b> JA/SAE	<b>Checked</b> DN

**Test No. SA1 - Test 2**

**Soil Infiltration Rate in Accordance with BR365**

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

$V_{p75-25}$

Initial parameters

Depth to water = **930 mm**      Average water depth: **235 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **470 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **400 mm**      Time interval: **71 min**

End time = **71 min**

Effective Storage Volume of Water in the Trial Pit = **0.615 m<sup>3</sup>**  
 75% Effective Depth = **1093 mm** from ground level  
 25% Effective Depth = **1298 mm** from ground level  
 Time at 75% Effective Depth = **3 minutes**  
 Time at 25% Effective Depth = **30 minutes**

= **0.31 m<sup>3</sup>**

= **2.77 m<sup>2</sup>**

= **1620 sec**

= **6.9E-05 m/sec**

Average Soakaway Rate = **1.7E-04 m<sup>3</sup>/sec**

Average soakaway area = **2.96 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$  **Soil Infiltration Rate = 6.9E-05 m/sec**  
**Average Infiltration Rate = 5.6E-05 m/sec**

$t_{p75-25}$

<b>PROJECT:</b>	<b>Wombwell High School</b>	<b>Job No.</b> 43497	<b>Date</b> 19.12.18
<b>SUBJECT:</b>	<b>Infiltration Test Results and Calculation of Infiltration Rates</b>	<b>Prepared</b> JA/SAE	<b>Checked</b> DN

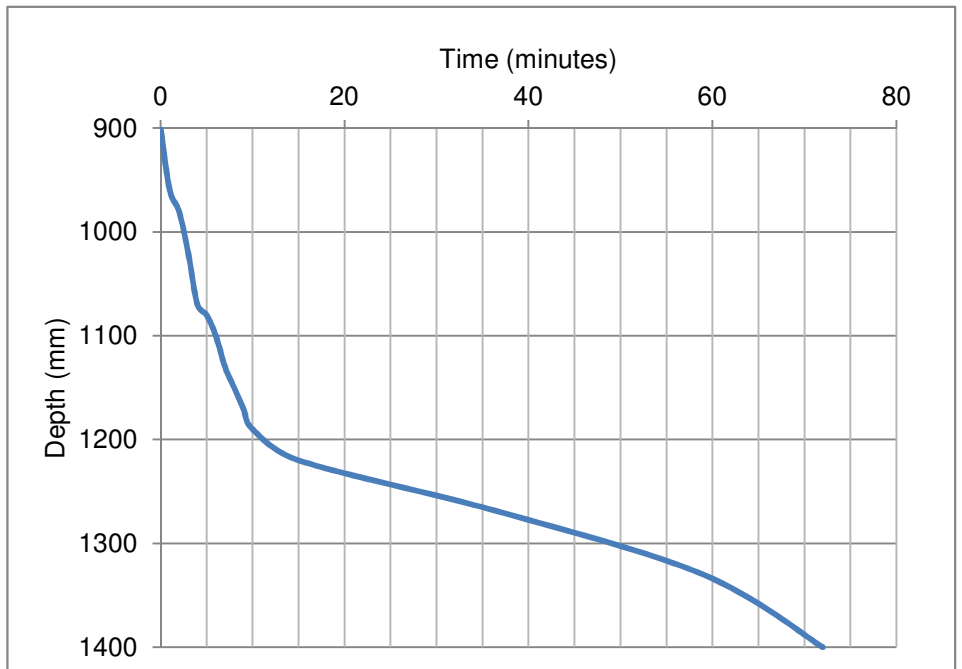
**Test No. SA1 - Test 3**

**Test Pit Dimensions**

Length = **2500** mm                                      Plan area = **1.5** m<sup>2</sup>  
 Width = **600** mm  
 Depth = **1400** mm (Total depth)

Approximate time to discharge water into the hole: **30** Seconds  
 Depth to water after completion of pumping: **900** mm

<b>Time (min)</b>	<b>Depth (mm)</b>
0	900
1	960
2	980
3	1020
4	1070
5	1080
6	1100
7	1130
8	1150
9	1170
10	1190
15	1220
37	1270
59	1330
72	1400



<b>Depth (m)</b>	<b>Description</b>
0.00 - 0.35	TOPSOIL: Grass over dark brown sandy CLAY.
0.35 - 0.60	MADE GROUND: Light brown / orange brown sandy reworked CLAY.
0.60 - 1.60	Brown clayey SAND and GRAVEL with occasional to frequent cobbles. Gravel is fine to coarse angular to sub-angular of sandstone.

<b>PROJECT:</b>	<b>Wombwell High School</b>	<b>Job No.</b> 43497	<b>Date</b> 19.12.18
<b>SUBJECT:</b>	<b>Infiltration Test Results and Calculation of Infiltration Rates</b>	<b>Prepared</b> JA/SAE	<b>Checked</b> DN

**Test No. SA1 - Test 3**

**Soil Infiltration Rate in Accordance with BR365**

Where:  $V_{p75-25}$  is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

$a_{p50}$  is the internal surface area of the trial pit up to 50% effective depth and including the base area

$t_{p75-25}$  is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **900 mm**      Average water depth: **250 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **500 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **400 mm**      Time interval: **72 min**

End time = **72 min**

Effective Storage Volume of Water in the Trial Pit = **0.66 m<sup>3</sup>**  
 75% Effective Depth = **1070 mm** from ground level  
 25% Effective Depth = **1290 mm** from ground level  
 Time at 75% Effective Depth = **4 minutes**  
 Time at 25% Effective Depth = **45 minutes**

= **0.33 m<sup>3</sup>**

= **2.86 m<sup>2</sup>**

= **2460 sec**

= **4.7E-05 m/sec**

Average Soakaway Rate = **1.7E-04 m<sup>3</sup>/sec**

Average soakaway area = **3.05 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$  **Soil Infiltration Rate = 4.7E-05 m/sec**  
 $\frac{V_{p75-25}}{a_{p50}}$  **average Infiltration Rate = 5.7E-05 m/sec**

$t_{p75-25}$

<b>PROJECT:</b>	<b>Wombwell High School</b>	<b>Job No.</b> 43497	<b>Date</b> 19.12.18
<b>SUBJECT:</b>	<b>Infiltration Test Results and Calculation of Infiltration Rates</b>	<b>Prepared</b> JA/SAE	<b>Checked</b> DN

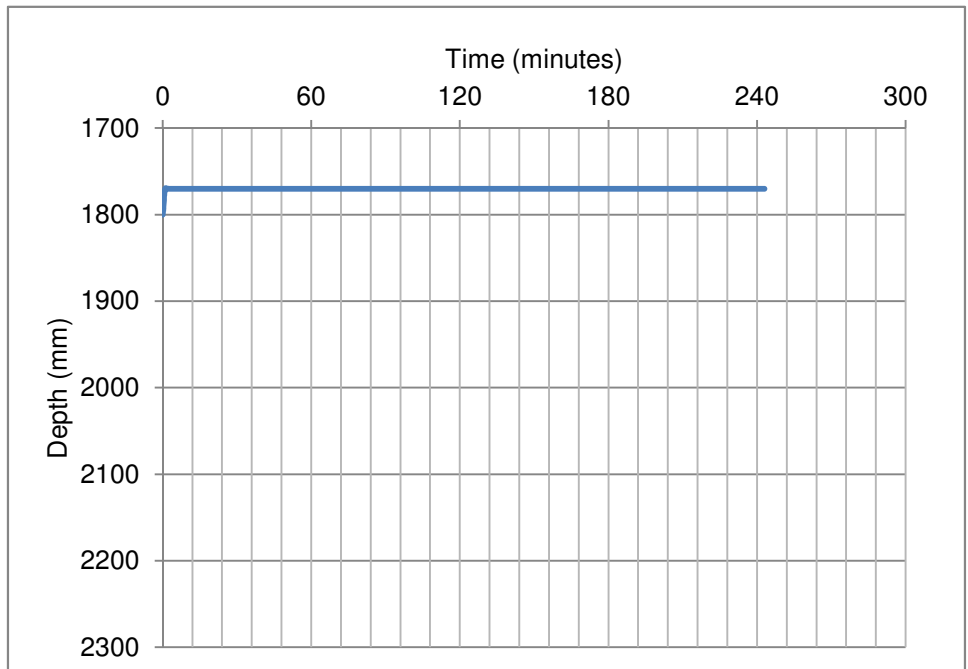
**Test No.** SA2 - Test 1

**Test Pit Dimensions**

Length = **2900 mm** Plan area = **1.74 m<sup>2</sup>**  
 Width = **600 mm**  
 Depth = **2250 mm (Total depth)**

Approximate time to discharge water into the hole: **30 Seconds**  
 Depth to water after completion of pumping: **1800 mm**

<b>Time (min)</b>	<b>Depth (mm)</b>
0	1800
1	1770
2	1770
3	1770
4	1770
5	1770
6	1770
7	1770
8	1770
9	1770
10	1770
20	1770
39	1770
112	1770
203	1770
243	1770



<b>Depth (m)</b>	<b>Description</b>
0.00 - 0.40	TOPSOIL: Grass over dark brown clayey SAND.
0.40 - 1.20	MADE GROUND: Firm brown sandy reworked CLAY.
1.20 - 1.80	MADE GROUND: Stiff to friable brown mottled grey sandy gravelly reworked CLAY with occasional cobbles. Gravel is medium to coarse angular to sub-angular of sandstone.
1.8-2.2	MADE GROUND: Grey brown friable sandy reworked CLAY.
2.2 - 2.25	Strong brown SANDSTONE.

<b>PROJECT:</b>	<b>Wombwell High School</b>	<b>Job No.</b> 43497	<b>Date</b> 19.12.18
<b>SUBJECT:</b>	<b>Infiltration Test Results and Calculation of Infiltration Rates</b>	<b>Prepared</b> JA/SAE	<b>Checked</b> DN

**Test No. SA2 - Test 1**

**Soil Infiltration Rate in Accordance with BR365**

Where:

$V_{p75-25}$  is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

$a_{p50}$  is the internal surface area of the trial pit up to 50% effective depth and including the base area

$t_{p75-25}$  is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **1770** mm  
Start time =  $a_{p50}$  **0** min

Average water depth: **480** mm

Change in water depth: **0** mm

Final parameters

Depth to water =  $t_{p75-25}$  **770** mm  
End time = **243** min

Time interval: **243** min

Effective Storage Volume of Water in the Trial Pit = **0.8352** m<sup>3</sup>  
75% Effective Depth = **1890** mm from ground level  
25% Effective Depth = **2130** mm from ground level  
Time at 75% Effective Depth = **N/A** minutes  
Time at 25% Effective Depth = **N/A** minutes

= **0.42** m<sup>3</sup>

= **3.42** m<sup>2</sup>

= **0** sec

= **N/A** m/sec

Average Soakaway Rate = **0.0E+00** m<sup>3</sup>/sec  
Average soakaway area = **5.10** m<sup>2</sup> (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$  **Soil Infiltration Rate** = **0.0E+00** m/sec  
**Average Infiltration Rate** = **0.0E+00** m/sec

$t_{p75-25}$



<b>PROJECT:</b>	<b>Wombwell High School</b>	<b>Job No.</b> 43497	<b>Date</b> 19.12.18
<b>SUBJECT:</b>	<b>Infiltration Test Results and Calculation of Infiltration Rates</b>	<b>Prepared</b> JA/SAE	<b>Checked</b> DN

**Test No. SA3 - Test 1**

**Soil Infiltration Rate in Accordance with BR365**

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

$V_{p75-25}$

Initial parameters

Depth to water = **1130 mm**  
Start time =  $a_{p50}$  **0 min**

Average water depth: **235 mm**

Change in water depth: **470 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **600 mm**  
End time = **7 min**

Time interval: **7 min**

Effective Storage Volume of Water in the Trial Pit = **0.6612 m<sup>3</sup>**  
75% Effective Depth = **1315 mm** from ground level  
25% Effective Depth = **1505 mm** from ground level  
Time at 75% Effective Depth = **2 minutes**  
Time at 25% Effective Depth = **5 minutes**

= **0.33 m<sup>3</sup>**

= **3.07 m<sup>2</sup>**

= **300 sec**

= **3.6E-04 m/sec**

Average Soakaway Rate = **1.9E-03 m<sup>3</sup>/sec**  
Average soakaway area = **3.39 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{a_{p50}}$  **Soil Infiltration Rate = 3.6E-04 m/sec**  
**verage Infiltration Rate = 5.8E-04 m/sec**

$t_{p75-25}$



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**Test No. SA3 - Test 2**

**Soil Infiltration Rate in Accordance with BR365**

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

$V_{p75-25}$

Initial parameters

Depth to water = **1130 mm**      Average water depth: **225 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **450 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **580 mm**      Time interval: **11 min**

End time = **11 min**

Effective Storage Volume of Water in the Trial Pit = **0.6786 m<sup>3</sup>**  
 75% Effective Depth = **1288 mm** from ground level  
 25% Effective Depth = **1483 mm** from ground level  
 Time at 75% Effective Depth = **3.5 minutes**  
 Time at 25% Effective Depth = **7.5 minutes**

= **0.34 m<sup>3</sup>**

= **3.11 m<sup>2</sup>**

= **450 sec**

= **2.4E-04 m/sec**

Average Soakaway Rate = **1.2E-03 m<sup>3</sup>/sec**

Average soakaway area = **3.32 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$  **Soil Infiltration Rate = 2.4E-04 m/sec**  
 $\frac{V_{p75-25}}{a_{p50}}$  **average Infiltration Rate = 3.6E-04 m/sec**

$t_{p75-25}$



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**Test No. SA3 - Test 3**

**Soil Infiltration Rate in Accordance with BR365**

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

$V_{p75-25}$

Initial parameters

Depth to water = **1020 mm**  
Start time =  $a_{p50}$  **1 min**

Average water depth: **265 mm**

Change in water depth: **530 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **550 mm**  
End time = **11 min**

Time interval: **10 min**

Effective Storage Volume of Water in the Trial Pit = **0.9222 m<sup>3</sup>**  
75% Effective Depth = **1153 mm** from ground level  
25% Effective Depth = **1418 mm** from ground level  
Time at 75% Effective Depth = **2 minutes**  
Time at 25% Effective Depth = **7 minutes**

= **0.46 m<sup>3</sup>**

= **3.60 m<sup>2</sup>**

= **420 sec**

= **3.1E-04 m/sec**

Average Soakaway Rate = **1.5E-03 m<sup>3</sup>/sec**  
Average soakaway area = **3.60 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$  **Soil Infiltration Rate = 3.1E-04 m/sec**  
**Average Infiltration Rate = 4.3E-04 m/sec**

$t_{p75-25}$



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**Test No. SA4 - Test 1**

**Soil Infiltration Rate in Accordance with BR365**

Where:  $V_{p75-25}$  is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

$a_{p50}$  is the internal surface area of the trial pit up to 50% effective depth and including the base area

$t_{p75-25}$  is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **990** mm      Average water depth: **255** mm

Start time =  $a_{p50}$  **0** min      Change in water depth: **510** mm

Final parameters

Depth to water =  $t_{p75-25}$  **500** mm      Time interval: **129** min

End time = **129** min

Effective Storage Volume of Water in the Trial Pit = **1.02765** m<sup>3</sup>  
 75% Effective Depth = **1118** mm from ground level  
 25% Effective Depth = **1373** mm from ground level  
 Time at 75% Effective Depth = **27** minutes  
 Time at 25% Effective Depth = **105** minutes

= **0.51** m<sup>3</sup>

= **3.93** m<sup>2</sup>

= **6300** sec

= **2.1E-05** m/sec

Average Soakaway Rate = **1.3E-04** m<sup>3</sup>/sec

Average soakaway area = **3.93** m<sup>2</sup> (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$  **Soil Infiltration Rate** = **2.1E-05** m/sec  
 $\frac{V_{p75-25}}{a_{p50}}$  **average Infiltration Rate** = **3.4E-05** m/sec

$t_{p75-25}$



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**Test No. SA4 - Test 2**

**Soil Infiltration Rate in Accordance with BR365**

Where:

$V_{p75-25}$  is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

$a_{p50}$  is the internal surface area of the trial pit up to 50% effective depth and including the base area

$t_{p75-25}$  is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **760 mm**      Average water depth: **330 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **520 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **280 mm**      Time interval: **98 min**

End time = **98 min**

Effective Storage Volume of Water in the Trial Pit = **1.14855 m<sup>3</sup>**  
 75% Effective Depth = **923 mm** from ground level  
 25% Effective Depth = **1208 mm** from ground level  
 Time at 75% Effective Depth = **32 minutes**  
 Time at 25% Effective Depth = **93 minutes**

= **0.57 m<sup>3</sup>**

= **4.15 m<sup>2</sup>**

= **5580 sec**

= **2.5E-05 m/sec**

Average Soakaway Rate = **1.8E-04 m<sup>3</sup>/sec**

Average soakaway area = **4.49 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$  **Soil Infiltration Rate = 2.5E-05 m/sec**  
 $\frac{V_{p75-25}}{a_{p50}}$  **average Infiltration Rate = 4.0E-05 m/sec**

$t_{p75-25}$



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**Test No. SA5 - Test 1**

**Soil Infiltration Rate in Accordance with BR365**

Where:

$V_{p75-25}$  is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

$a_{p50}$  is the internal surface area of the trial pit up to 50% effective depth and including the base area

$t_{p75-25}$  is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **1330 mm**  
Start time =  $a_{p50}$  **0 min**

Average water depth: **235 mm**

Change in water depth: **470 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **800 mm**  
End time = **63 min**

Time interval: **63 min**

Effective Storage Volume of Water in the Trial Pit = **0.8372 m<sup>3</sup>**  
75% Effective Depth = **1455 mm** from ground level  
25% Effective Depth = **1685 mm** from ground level  
Time at 75% Effective Depth = **11 minutes**  
Time at 25% Effective Depth = **46 minutes**

= **0.42 m<sup>3</sup>**

= **3.41 m<sup>2</sup>**

= **2760 sec**

= **4.5E-05 m/sec**

Average Soakaway Rate = **2.3E-04 m<sup>3</sup>/sec**  
Average soakaway area = **3.44 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$  **Soil Infiltration Rate = 4.5E-05 m/sec**  
 $\frac{V_{p75-25}}{a_{p50}}$  **average Infiltration Rate = 6.6E-05 m/sec**

$t_{p75-25}$



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**Test No. SA5 - Test 2**

**Soil Infiltration Rate in Accordance with BR365**

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

Where:  $V_{p75-25}$  is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$a_{p50}$  is the internal surface area of the trial pit up to 50% effective depth and including the base area

$t_{p75-25}$  is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **1270 mm**      Average water depth: **200 mm**  
 Start time = **10 min**      Change in water depth: **400 mm**

Final parameters

Depth to water = **1670 mm**      Time interval: **114 min**  
 End time = **124 min**

Effective Storage Volume of Water in the Trial Pit = **0.8008 m<sup>3</sup>**  
 75% Effective Depth = **1340 mm** from ground level  
 25% Effective Depth = **1560 mm** from ground level  
 Time at 75% Effective Depth = **26 minutes**  
 Time at 25% Effective Depth = **109 minutes**

$V_{p75-25}$  = **0.40 m<sup>3</sup>**  
 $a_{p50}$  = **3.34 m<sup>2</sup>**  
 $t_{p75-25}$  = **6540 sec**  
 $f$  = **1.8E-05 m/sec**

Average Soakaway Rate = **1.1E-04 m<sup>3</sup>/sec**  
 Average soakaway area = **3.20 m<sup>2</sup>** (sides + base)

**BR365 Soil Infiltration Rate = 1.8E-05 m/sec**  
**Average Infiltration Rate = 3.3E-05 m/sec**



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**Test No. SA6 - Test 1**

**Soil Infiltration Rate in Accordance with BR365**

Where:

$V_{p75-25}$  is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

$a_{p50}$  is the internal surface area of the trial pit up to 50% effective depth and including the base area

$t_{p75-25}$  is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **830 mm**      Average water depth: **235 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **470 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **300 mm**      Time interval: **14 min**

End time = **14 min**

Effective Storage Volume of Water in the Trial Pit = **0.924 m<sup>3</sup>**  
 75% Effective Depth = **970 mm** from ground level  
 25% Effective Depth = **1190 mm** from ground level  
 Time at 75% Effective Depth = **4.5 minutes**  
 Time at 25% Effective Depth = **9.5 minutes**

= **0.46 m<sup>3</sup>**

= **3.73 m<sup>2</sup>**

= **570 sec**

= **2.2E-04 m/sec**

Average Soakaway Rate = **1.2E-03 m<sup>3</sup>/sec**

Average soakaway area = **3.84 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$  **Soil Infiltration Rate = 2.2E-04 m/sec**  
**Average Infiltration Rate = 3.1E-04 m/sec**

$t_{p75-25}$



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**Test No. SA6 - Test 2**

**Soil Infiltration Rate in Accordance with BR365**

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

$V_{p75-25}$

Initial parameters

Depth to water = **710 mm**      Average water depth: **245 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **490 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **200 mm**      Time interval: **24 min**

End time = **24 min**

Effective Storage Volume of Water in the Trial Pit = **0.966 m<sup>3</sup>**  
 75% Effective Depth = **855 mm** from ground level  
 25% Effective Depth = **1085 mm** from ground level  
 Time at 75% Effective Depth = **6.5 minutes**  
 Time at 25% Effective Depth = **18 minutes**

= **0.48 m<sup>3</sup>**

= **3.80 m<sup>2</sup>**

= **1080 sec**

= **1.2E-04 m/sec**

Average Soakaway Rate = **7.1E-04 m<sup>3</sup>/sec**

Average soakaway area = **3.91 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$  **Soil Infiltration Rate = 1.2E-04 m/sec**  
 $\frac{V_{p75-25}}{a_{p50}}$  **average Infiltration Rate = 1.8E-04 m/sec**

$t_{p75-25}$



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**Test No. SA6 - Test 3**

**Soil Infiltration Rate in Accordance with BR365**

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

$V_{p75-25}$

Initial parameters

Depth to water = **740 mm**      Average water depth: **230 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **460 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **200 mm**      Time interval: **26 min**

End time = **26 min**

Effective Storage Volume of Water in the Trial Pit = **0.945 m<sup>3</sup>**  
 75% Effective Depth = **863 mm** from ground level  
 25% Effective Depth = **1088 mm** from ground level  
 Time at 75% Effective Depth = **7 minutes**  
 Time at 25% Effective Depth = **18 minutes**

= **0.47 m<sup>3</sup>**

= **3.77 m<sup>2</sup>**

= **1080 sec**

= **1.2E-04 m/sec**

Average Soakaway Rate = **6.2E-04 m<sup>3</sup>/sec**

Average soakaway area = **3.80 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$  **5 Soil Infiltration Rate = 1.2E-04 m/sec**  
 $\frac{V_{p75-25}}{a_{p50}}$  **verage Infiltration Rate = 1.6E-04 m/sec**

$t_{p75-25}$



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**Test No. SA7 - Test 1**

**Soil Infiltration Rate in Accordance with BR365**

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

$V_{p75-25}$

Initial parameters

Depth to water = **680 mm**      Average water depth: **260 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **520 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **200 mm**      Time interval: **121 min**

End time = **121 min**

Effective Storage Volume of Water in the Trial Pit = **1.24 m<sup>3</sup>**  
 75% Effective Depth = **825 mm** from ground level  
 25% Effective Depth = **1075 mm** from ground level  
 Time at 75% Effective Depth = **18 minutes**  
 Time at 25% Effective Depth = **70 minutes**

= **0.62 m<sup>3</sup>**

= **4.43 m<sup>2</sup>**

= **4200 sec**

= **3.3E-05 m/sec**

Average Soakaway Rate = **1.8E-04 m<sup>3</sup>/sec**

Average soakaway area = **4.51 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$  **Soil Infiltration Rate = 3.3E-05 m/sec**  
**Average Infiltration Rate = 3.9E-05 m/sec**

$t_{p75-25}$



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**Test No. SA7 - Test 2**

**Soil Infiltration Rate in Accordance with BR365**

Where:  $V_{p75-25}$  is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

$a_{p50}$  is the internal surface area of the trial pit up to 50% effective depth and including the base area

$t_{p75-25}$  is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **910 mm**      Average water depth: **230 mm**

Start time =  $a_{p50}$  **10 min**      Change in water depth: **320 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **230 mm**      Time interval: **126 min**

End time = **136 min**

Effective Storage Volume of Water in the Trial Pit = **1.0912 m<sup>3</sup>**  
 75% Effective Depth = **970 mm** from ground level  
 25% Effective Depth = **1190 mm** from ground level  
 Time at 75% Effective Depth = **34 minutes**  
 Time at 25% Effective Depth = **128 minutes**

= **0.55 m<sup>3</sup>**

= **4.20 m<sup>2</sup>**

= **7680 sec**

= **1.7E-05 m/sec**

Average Soakaway Rate = **1.0E-04 m<sup>3</sup>/sec**

Average soakaway area = **4.27 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$  **Soil Infiltration Rate = 1.7E-05 m/sec**  
 $\frac{V_{p75-25}}{a_{p50}}$  **average Infiltration Rate = 2.5E-05 m/sec**

$t_{p75-25}$



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**Test No. SA8 - Test 1**

**Soil Infiltration Rate in Accordance with BR365**

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

$V_{p75-25}$

Initial parameters

Depth to water = **810 mm**      Average water depth: **445 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **90 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **900 mm**      Time interval: **236 min**

End time = **236 min**

Effective Storage Volume of Water in the Trial Pit = **1.0752 m<sup>3</sup>**  
 75% Effective Depth = **940 mm** from ground level  
 25% Effective Depth = **1180 mm** from ground level  
 Time at 75% Effective Depth = **N/A** minutes  
 Time at 25% Effective Depth = **N/A** minutes

= **0.54 m<sup>3</sup>**

= **4.11 m<sup>2</sup>**

= **0 sec**

= **#DIV/0! m/sec**

Average Soakaway Rate = **1.4E-05 m<sup>3</sup>/sec**

Average soakaway area = **5.71 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$  **Soil Infiltration Rate = UTC m/sec**  
**verage Infiltration Rate = 2.5E-06 m/sec**

$t_{p75-25}$



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**Test No. SA9 - Test 1**

**Soil Infiltration Rate in Accordance with BR365**

Where:  $V_{p75-25}$  is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

$a_{p50}$  is the internal surface area of the trial pit up to 50% effective depth and including the base area

$t_{p75-25}$  is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **760 mm**      Average water depth: **245 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **490 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **250 mm**      Time interval: **45 min**

End time = **45 min**

Effective Storage Volume of Water in the Trial Pit = **1.0528 m<sup>3</sup>**  
 75% Effective Depth = **898 mm** from ground level  
 25% Effective Depth = **1133 mm** from ground level  
 Time at 75% Effective Depth = **3 minutes**  
 Time at 25% Effective Depth = **22 minutes**

= **0.53 m<sup>3</sup>**

= **4.07 m<sup>2</sup>**

= **1320 sec**

= **9.8E-05 m/sec**

Average Soakaway Rate = **4.1E-04 m<sup>3</sup>/sec**

Average soakaway area = **4.15 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$  **Soil Infiltration Rate = 9.8E-05 m/sec**  
**Average Infiltration Rate = 9.8E-05 m/sec**

$t_{p75-25}$



<b>PROJECT:</b>	<b>Wombwell High School</b>	<b>Job No.</b> 43497	<b>Date</b> 19.12.18
<b>SUBJECT:</b>	<b>Infiltration Test Results and Calculation of Infiltration Rates</b>	<b>Prepared</b> SAE	<b>Checked</b> DN

**Test No. SA9 - Test 2**

**Soil Infiltration Rate in Accordance with BR365**

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

$V_{p75-25}$

Initial parameters

Depth to water = **700 mm**      Average water depth: **275 mm**

Start time =  $a_{p50}$  **0 min**      Change in water depth: **550 mm**

Final parameters

Depth to water =  $t_{p75-25}$  **250 mm**      Time interval: **62 min**

End time = **62 min**

Effective Storage Volume of Water in the Trial Pit = **1.2096 m<sup>3</sup>**  
 75% Effective Depth = **845 mm** from ground level  
 25% Effective Depth = **1115 mm** from ground level  
 Time at 75% Effective Depth = **6 minutes**  
 Time at 25% Effective Depth = **36 minutes**

= **0.60 m<sup>3</sup>**

= **4.35 m<sup>2</sup>**

= **2160 sec**

= **6.4E-05 m/sec**

Average Soakaway Rate = **3.3E-04 m<sup>3</sup>/sec**

Average soakaway area = **4.39 m<sup>2</sup>** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$  **Soil Infiltration Rate = 6.4E-05 m/sec**  
Average Infiltration Rate = 7.6E-05 m/sec

$t_{p75-25}$



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<b>SUBJECT:</b>	<b>Infiltration Test Results and Calculation of Infiltration Rates</b>	<b>Prepared</b> <b>SAE</b>	<b>Checked</b> <b>DN</b>

**Test No. SA9 - Test 3**

**Soil Infiltration Rate in Accordance with BR365**

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

Where:  $V_{p75-25}$  is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$a_{p50}$  is the internal surface area of the trial pit up to 50% effective depth and including the base area

$t_{p75-25}$  is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **690** mm      Average water depth: **280** mm  
 Start time = **0** min      Change in water depth: **560** mm

Final parameters

Depth to water = **1250** mm      Time interval: **60** min  
 End time = **60** min

Effective Storage Volume of Water in the Trial Pit = **1.2096** m<sup>3</sup>  
 75% Effective Depth = **845** mm from ground level  
 25% Effective Depth = **1115** mm from ground level  
 Time at 75% Effective Depth = **9** minutes  
 Time at 25% Effective Depth = **38** minutes

$V_{p75-25}$  = **0.60** m<sup>3</sup>

$a_{p50}$  = **4.35** m<sup>2</sup>

$t_{p75-25}$  = **2280** sec

$f$  = **6.1E-05** m/sec

Average Soakaway Rate = **3.5E-04** m<sup>3</sup>/sec  
 Average soakaway area = **4.42** m<sup>2</sup> (sides + base)

**BR365 Soil Infiltration Rate** = **6.1E-05** m/sec  
**Average Infiltration Rate** = **7.9E-05** m/sec

End of Report