



**Design it**

**Structural Solutions Ltd**



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Job Ref.

22/001

Rev.

0

Date.

Nov 22

**Calculations for:**

**BMBC Housing Growth  
Dev. Goldthorpe, Barnsley**

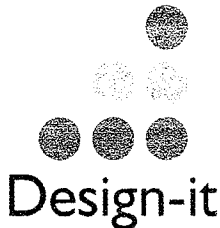
**External Works –  
Proposed Retaining Wall Designs**

**Prepared By:**


**Ian R Thorpe**

BEng (Hons) CEng MStructE

**November 2022**

	Project	Dev. Goldthorpe Markets, Barnsley			Job Ref
	Section	External Works – Retaining Walls			22001
	Calc By	Date	Checked	Date	Sht No.
	I.T.	Nov 22	I.T.	Nov 22	1

Ref		Output
	<p><b><u>Design Statement</u></b></p> <p>It is proposed to build new housing on a development on the market area and carpark in Goldthorpe Town Centre, as indicated on the attached site plan.</p> <p>The proposed development is to comprise 9 properties with 4 different house types. A single semi-detached bungalow, a single detached bungalow, 2 detached 2 storey houses and 2 semi-detached 2 storey house.</p> <p><b>External Walls</b></p> <p>From the site investigation report allowable bearing pressures of 100kN/m<sup>2</sup> are to be adopted. There are level differences requiring built up retaining walls between plots 7&amp;8. Wall will support surcharge from driveway in final condition.</p> <p>Gardens are to be built up to plot 9 above the level of the existing access to the rear of terrace houses along the boundary line. Approx level will increase towards the rear boundary to plot 9 of approx. 600mm to 700mm. A 6ft panel fence, (to Architects details), is to be built above the wall. The wall will be thickened out at post locations with posts embedded into the ground by a min 600mm. Moment forces from the fence will be transferred direct to ground.</p> <p>(Refer to extract of Plots 7, 8 &amp; 9 for locations.)</p> <p><b><u>Notes</u></b></p> <p><b><i>Dimensions defined in these calculations are taken from Architects details, and are defined here-in for design purposes <u>only</u>.</i></b></p> <p><b><i>Any variations to the proposed drawing details are to be notified to check proposed design details / requirements</i></b></p> <p><b><u><i>It is a requirement to submit all design calculations to building control for checking and approval prior to works commencing.</i></u></b></p>	

	Project	Dev. Goldthorpe Markets, Barnsley			Job Ref
	Section	External Works – Retaining Walls			22001
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Ref				Output
	<b><u>Loadings (BS 6399 Pt 1)</u></b>			
	<b>Dead</b>		<b>kN/m<sup>2</sup></b>	
	Surcharge Loads	Driveways & roads + construction loads on roads	<b>10</b>	
		Gardens – No traffic, No Access Gravel backfill No compaction	<b>2.5 - 5</b>	
	Densities	Walls - Masonry	<b>10</b>	
		Soil	<b>18</b>	
		Concrete	<b>24</b>	
		Water	<b>10</b>	

FOR EXTENT OF RETAINING WALLS AND  
PROPOSED BOUNDARY TREATMENTS  
REFER TO BMBC DRGS.

RW-B  
REFER TO DIT-DRG  
21153/EX/01

RW-B  
REFER TO DIT-DRG  
21153/EX/01

FOR PLOTS 8 & 9  
FOUNDATION DETAILS REF  
TO DIT-DRG 21153/FN/07

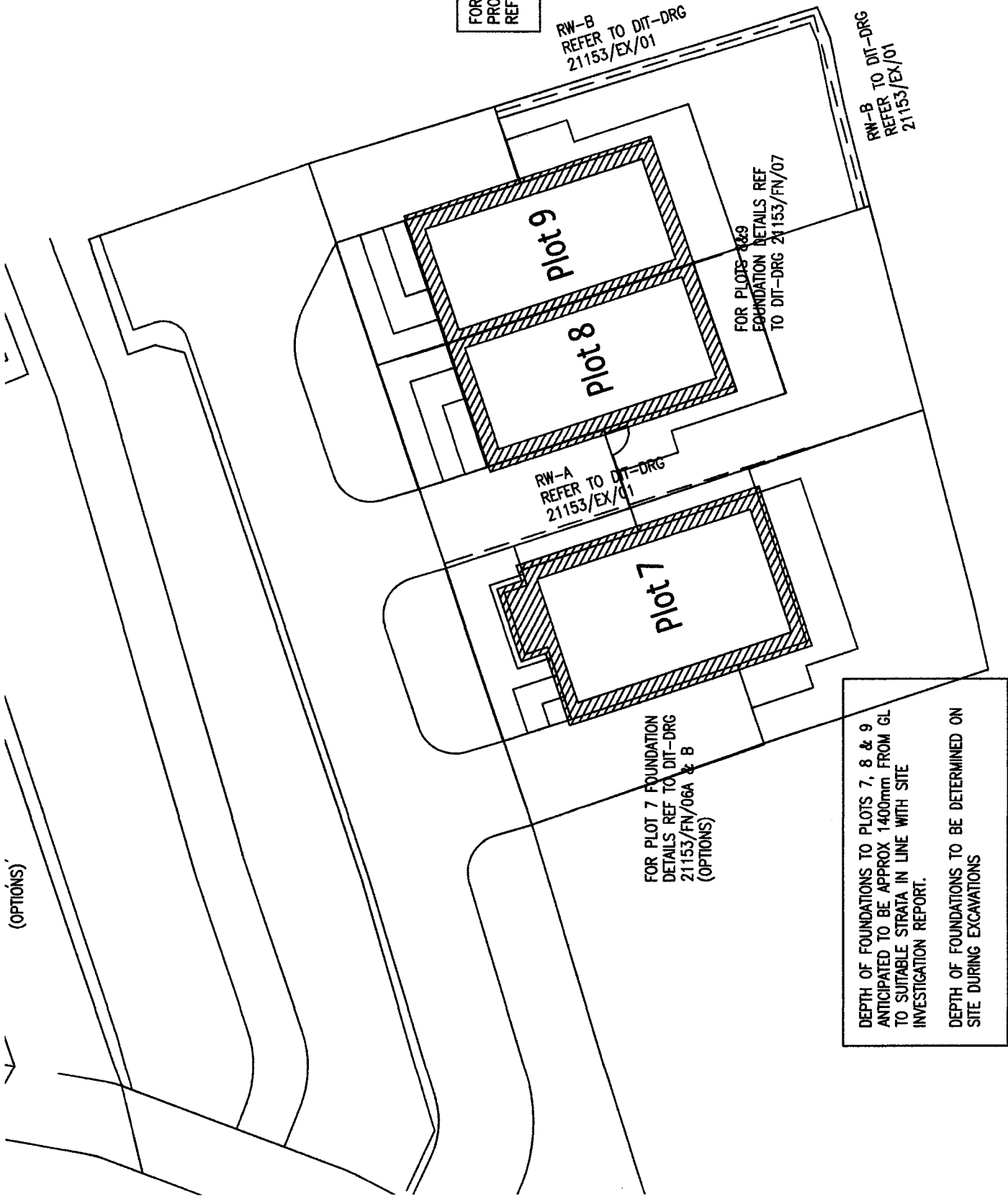
RW-A  
REFER TO DIT-DRG  
21153/EX/01

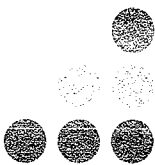
FOR PLOT 7 FOUNDATION  
DETAILS REF TO DIT-DRG  
21153/FN/06A & B  
(OPTIONS)

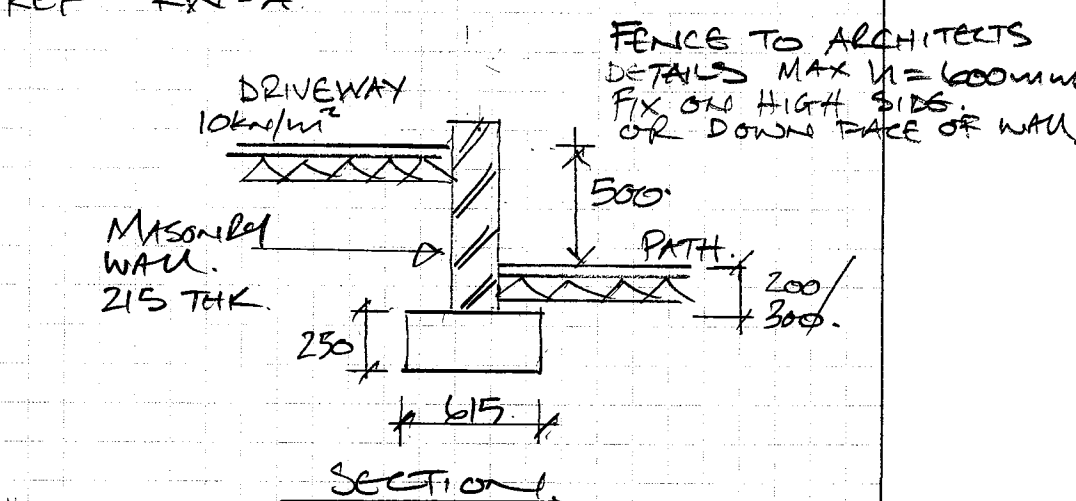
DEPTH OF FOUNDATIONS TO PLOTS 7, 8 & 9  
ANTICIPATED TO BE APPROX 1400mm FROM GL  
TO SUITABLE STRATA IN LINE WITH SITE  
INVESTIGATION REPORT.

DEPTH OF FOUNDATIONS TO BE DETERMINED ON  
SITE DURING EXCAVATIONS

(OPTIONS)



 Design-it	Project	DEV. GOLDTHORPE MARKETS.			Job Ref
	Section	EXTERNAL WORKS - WALLS.			22001
	Calc By	Date	Checked	Date	Sht No.
	IT	NOV 22	IT	NOV 22.	4

Ref	Output
	<p>WALL BETWEEN PLOTS 7 &amp; 8.</p> <p>REF R/W-A</p>  <p>SECTION 1.</p> <p>NOTE WALL MAY BE MIRRORED TO SUIT LEVELS.</p> <p>REFER TO SHTS FOR WALL DESIGN</p> <p>NOTE HOUSE FOUNDATIONS MIN DEPTH TO PLOTS TO BE 1400mm. NO LATERAL SURCHARGE.</p>

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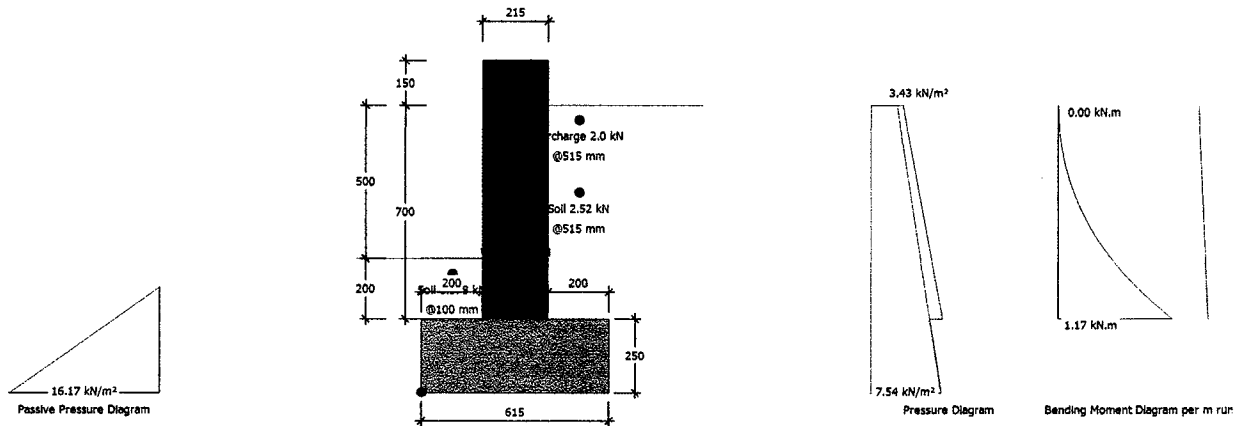
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Sheet : /  
Made by :  
Date : 14 December 2022 / Ver. 2021.08.26  
Checked :  
Approved :



MasterKey : Retaining Wall Design to BS 8002 : 1994, BS EN 1996-1-1:2005+A1:2012 and BS 8110 : 1997

## Boundary wall 500

### Gravity Masonry Retaining Wall with Un-Reinforced Concrete Base

**Summary of Design Data****Notes**

Material Densities (kN/m³)  
Concrete grade  
Surcharge and Water Table  
Unplanned excavation depth

All dimensions are in mm and all forces are per metre run  
Soil 18.00, Concrete 24.00, Masonry 20.00  
fcu 30 N/mm², Permissible tensile stress 0.250 N/mm²  
Surcharge 10.00 kN/m², Fully drained  
Front of wall 95 mm

**Soil Properties**

Bearing pressure  
Back Soil Friction and Cohesion  
Base Friction and Cohesion  
Front Soil Friction and Cohesion

Permissible service pressure @ front 100.00 kN/m², @ back 100.00 kN/m²  
 $\phi = \text{Atn}(\tan(34)/1.2) = 29.34^\circ$   
 $\delta = \text{Atn}(0.75 \times \tan(\text{Atn}(\tan(34)/1.2))) = 22.86^\circ$   
 $\phi = \text{Atn}(\tan(30)/1.2) = 25.69^\circ$

**Loading Cases**

G<sub>Soil</sub>- Soil Self Weight, G<sub>Wall</sub>- Wall & Base Self Weight, F<sub>vHeel</sub>- Vertical Loads over Heel,

P<sub>a</sub>- Active Earth Pressure, P<sub>surcharge</sub>- Earth pressure from surcharge, P<sub>p</sub>- Passive Earth Pressure

Case 1: Geotechnical Design

1.00 G<sub>Soil</sub>+1.00 G<sub>Wall</sub>+1.00 F<sub>vHeel</sub>+1.00 P<sub>a</sub>+1.00 P<sub>surcharge</sub>+1.00 P<sub>p</sub>

Case 2: Structural Ultimate Design

1.40 G<sub>Soil</sub>+1.40 G<sub>Wall</sub>+1.60 F<sub>vHeel</sub>+1.00 P<sub>a</sub>+1.00 P<sub>surcharge</sub>+1.00 P<sub>p</sub>

**Geotechnical Design****Wall Stability - Virtual Back Pressure**

Case 1 Overturning/Stabilising	1.986/4.626	0.429	OK
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**Wall Sliding - Virtual Back Pressure**

Fx/(R <sub>xFriction</sub> + R <sub>xPassive</sub> )	4.935/(5.162+2.878)	0.614	OK
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**Soil Pressure**

Virtual Back (No uplift)	Max(37.760/100, 2.057/100) kN/m²	0.378	OK
Wall Back (No uplift)	Max(38.487/100, 1.331/100) kN/m²	0.385	OK

**Structural Design****Masonry Wall Details**

Partial Safety Factor (γ <sub>mc</sub> /γ <sub>mf</sub> )	Units Category II, Execution Control Class 2	3/2.7	Table NA.1
Material	Clay bricks with water absorption between 7% and 12%		
Units and Mortar Strength	5 N/mm². Mortar designation M12/(i)		
Compressive Strength (f <sub>k</sub> )	Group 1, γ=20 kN/m³	2.5 N/mm²	Table NA.4

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**Wall Design (Inner Face Tension)**

Critical Section	Critical @ 0 mm from base, Case 2		
Section Properties @ Base	t=215 mm, Area=2150 cm <sup>2</sup> , Zb=7704 cm <sup>3</sup>		
Flexural Strength $f_{xkl}$	$f_{xkl}=0.5$ , $gd=0.017$ N/mm <sup>2</sup> , $f_{xkl}=f_{xkl}+0.9$ gd.γmf	0.541 N/mm <sup>2</sup>	Table NA.6
$Mr=f_{xkl}.Zb/γmf$	0.541x7704/2.7	1.54 kN.m	
Moment Capacity Check (M/Mr)	M 1.2 kN.m, Mr 1.5 kN.m	0.762	OK
Shear Capacity Check	F 3.6 kN, $f_{vk}0.307$ N/mm <sup>2</sup> , Fvr 26.4 kN	0.14	OK

**Base Top Face Tension**

Maximum Tensile Stress	M 0.452, h 250, fcu 30, Permissible 0.25 N/mm <sup>2</sup>	0.04 N/mm <sup>2</sup>	OK
Shear Capacity Check	F 4.3 kN, vc 0.350 N/mm <sup>2</sup> , Fvr 43.8 kN	0.10	OK

**Base Bottom Face Tension**

Maximum Tensile Stress	M 0.534, h 250, fcu 30, Permissible 0.25 N/mm <sup>2</sup>	0.05 N/mm <sup>2</sup>	OK
Shear Capacity Check	F 5.1 kN, vc 0.350 N/mm <sup>2</sup> , Fvr 43.8 kN	0.12	OK

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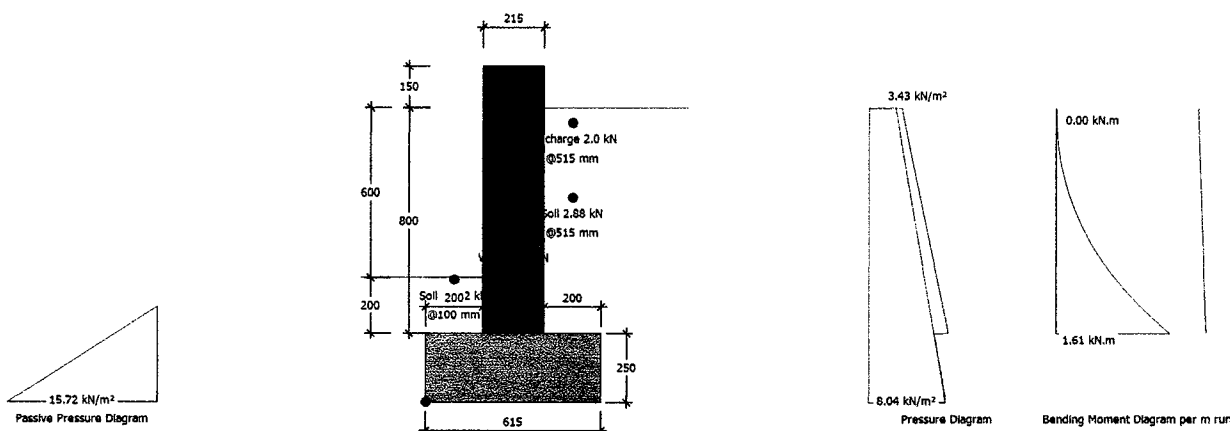
Checked :

Approved :

MasterKey : Retaining Wall Design to BS 8002 : 1994, BS EN 1996-1-1:2005+A1:2012 and BS 8110 : 1997

## Boundary wall 600 Max

### Reinforced Masonry Retaining Wall with Un-Reinforced Concrete Base

**Summary of Design Data****Notes**

Material Densities (kN/m³)

Concrete grade

Reinforcement design

Surcharge and Water Table

Unplanned excavation depth

† The Engineer must satisfy him/herself to the reinforcement detailing requirements of the relevant codes of practice

All dimensions are in mm and all forces are per metre run

Soil 18.00, Concrete 24.00, Masonry 20.00

fcu 30 N/mm², Permissible tensile stress 0.250 N/mm²

fy 460 N/mm², fyb 460 N/mm² designed to BS 8110: 1997

Surcharge 10.00 kN/m², Fully drained

Front of wall 105 mm

**Soil Properties**

Bearing pressure

Back Soil Friction and Cohesion

Base Friction and Cohesion

Front Soil Friction and Cohesion

Premissable service pressure @ front 100.00 kN/m², @ back 100.00 kN/m²

 $\alpha_h = \text{Atn}(\tan(34)/1.2) = 29.34^\circ$  $\delta = \text{Atn}(0.75 \times \tan(\text{Atn}(\tan(34)/1.2))) = 22.86^\circ$  $\phi = \text{Atn}(\tan(30)/1.2) = 25.69^\circ$ **Loading Cases**G<sub>Soil</sub>- Soil Self Weight, G<sub>Wall</sub>- Wall & Base Self Weight, F<sub>VHeel</sub>- Vertical Loads over Heel,P<sub>a</sub>- Active Earth Pressure, P<sub>surcharge</sub>- Earth pressure from surcharge, P<sub>p</sub>- Passive Earth PressureCase 1: Geotechnical Design 1.00 G<sub>Soil</sub>+1.00 G<sub>Wall</sub>+1.00 F<sub>VHeel</sub>+1.00 P<sub>a</sub>+1.00 P<sub>surcharge</sub>+1.00 P<sub>p</sub>Case 2: Structural Ultimate Design 1.40 G<sub>Soil</sub>+1.40 G<sub>Wall</sub>+1.60 F<sub>VHeel</sub>+1.00 P<sub>a</sub>+1.00 P<sub>surcharge</sub>+1.00 P<sub>p</sub>**Geotechnical Design****Wall Stability - Virtual Back Pressure**

Case 1 Overturning/Stabilising 2.517/4.940

0.509

OK

**Wall Sliding - Virtual Back Pressure**Fx/(R<sub>XFriction</sub>+ R<sub>XPassive</sub>) 5.713/(5.480+2.719)

0.697

OK

**Soil Pressure**

Virtual Back 46.473/100 kN/m², Length under pressure 0.559 m

0.465

OK

Wall Back 50.323/100 kN/m², Length under pressure 0.517 m

0.503

OK



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**Structural Design****Masonry Wall Details**

Partial Safety Factor ( $\gamma_{mc}/\gamma_{mf}$ )	Units Category II, Execution Control Class 2	3/2.7	Table NA.1
Material	Clay bricks with water absorption less than 7%		
Units and Mortar Strength	10 N/mm <sup>2</sup> , Mortar designation M12/(i)		
Compressive Strength ( $f_k$ )	Group 1, $\gamma=20$ kN/m <sup>3</sup>	5.0 N/mm <sup>2</sup>	Table NA.4

**Wall Design (Inner Face Tension)**


Critical Section	Critical @ 0 mm from base, Case 2		
Section Properties @ Base	$t=215$ mm, Area=2150 cm <sup>2</sup> , Zb=7704 cm <sup>3</sup>		
Flexural Strength $f_{xk1}$	$f_{xk1}=0.7$ , $gd=0.019$ N/mm <sup>2</sup> , $f_{xk1}=f_{xk1}+0.9$ gd. $\gamma_{mf}$	0.746 N/mm <sup>2</sup>	Table NA.6
$M_r=f_{xk1} \cdot Z_b/\gamma_{mf}$	0.746x7704/2.7	2.13 kN.m	
Moment Capacity Check (M/M <sub>r</sub> )	M 1.6 kN.m, M <sub>r</sub> 2.1 kN.m	0.755	OK
Shear Capacity Check	F 4.5 kN, $f_{vk}0.308$ N/mm <sup>2</sup> , F <sub>vr</sub> 26.5 kN	0.17	OK

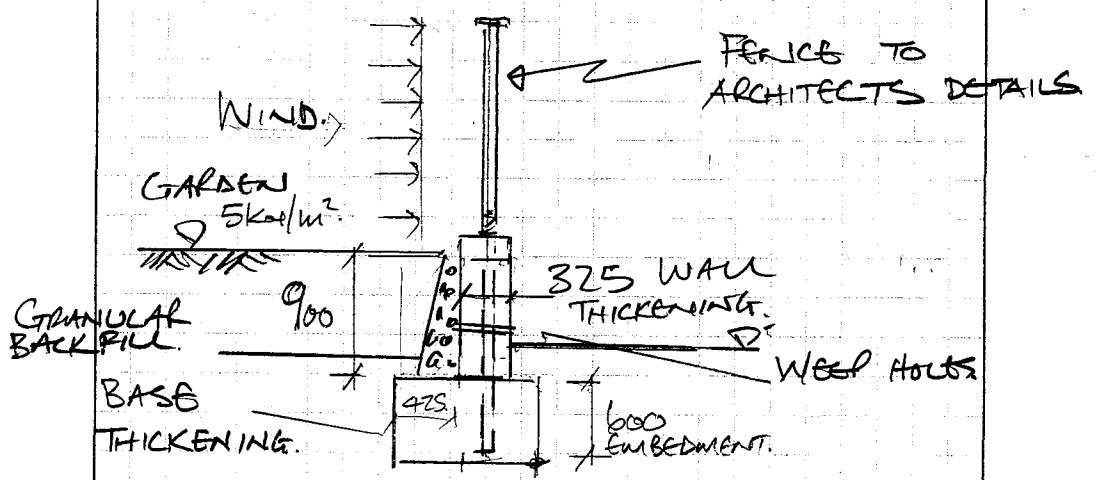
**Base Top Face Tension**

Maximum Tensile Stress	M 0.608, h 250, fcu 30, Permissible 0.25 N/mm <sup>2</sup>	0.06 N/mm <sup>2</sup>	OK
Shear Capacity Check	F 5.7 kN, vc 0.350 N/mm <sup>2</sup> , F <sub>vr</sub> 43.8 kN	0.13	OK

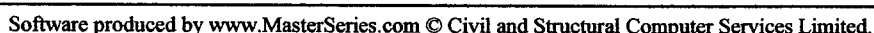
**Base Bottom Face Tension**

Maximum Tensile Stress	M 0.711, h 250, fcu 30, Permissible 0.25 N/mm <sup>2</sup>	0.07 N/mm <sup>2</sup>	OK
Shear Capacity Check	F 6.7 kN, vc 0.350 N/mm <sup>2</sup> , F <sub>vr</sub> 43.8 kN	0.15	OK

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	Section	EXTERNAL WORKS - WATTS.			22001
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Ref	Output
	<p><u>BOUNDARY WALL - PLOT 9.</u></p> <p>STATEMENT:- BOUNDARY RETAINING WALL, MASONRY CONSTRUCTION WITH 1830mm FENCE ABOVE. FENCE SPANS BETWEEN POSTS SECURED INTO WALL THICKENINGS. &amp; EMBEDDED A MIN 600mm</p> <p>REF RW-B ON PLAN.</p>  <p>WALL TO REAR OF PLOT. RETAINED HEIGHT REDUCES UP TO HOUSE PROXIMITY OF HOUSE IS GREATER THAN DEPTH OF SUPPORT PLUS BASE. NO LATERAL SURCHARGE.</p>

**Garden Boundary wall 700 215 thk  
Reinforced Masonry Retaining Wall with Reinforced Concrete Base**



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**Structural Design****Masonry Wall Details**

Partial Safety Factor ( $\gamma_{mc}/\gamma_{mf}$ )	Units Category II, Execution Control Class 2	3/2.7	Table NA.1
Material	Clay bricks with water absorption between 7% and 12%		
Units and Mortar Strength	5 N/mm <sup>2</sup> . Mortar designation M12/(i)		
Compressive Strength ( $f_k$ )	Group 1, $\gamma=20$ kN/m <sup>3</sup>	2.5 N/mm <sup>2</sup>	Table NA.4

**Wall Design (Inner Face Tension)**

Critical Section	Critical @ 0 mm from base, Case 2		
Section Properties @ Base	$t=225$ mm, Area=2250 cm <sup>2</sup> , $Z_b=8438$ cm <sup>3</sup>		
Flexural Strength $f_{xk1}$	$f_{xk1}=0.5$ , $gd=0.021$ N/mm <sup>2</sup> , $f_{xk1}=f_{xk1}+0.9$ gd. $\gamma_{mf}$	0.551 N/mm <sup>2</sup>	Table NA.6
$M_r=f_{xk1}.Z_b/\gamma_{mf}$	$0.551 \times 8438 / 2.7$	1.72 kN.m	
Moment Capacity Check (M/M <sub>r</sub> )	M 1.5 kN.m, M <sub>r</sub> 1.7 kN.m	0.865	OK
Shear Capacity Check	F 4.0 kN, $f_{vk}0.308$ N/mm <sup>2</sup> , F <sub>vr</sub> 27.8 kN	0.14	OK

**Base Top Face Tension**

Maximum Tensile Stress	M 0.854, h 250, f <sub>cu</sub> 30, Permissible 0.25 N/mm <sup>2</sup>	0.08 N/mm <sup>2</sup>	OK
Shear Capacity Check	F 4.9 kN, $v_c$ 0.350 N/mm <sup>2</sup> , F <sub>vr</sub> 43.8 kN	0.11	OK

**Base Bottom Steel Design**

Steel Provided (Cover)	Main B10@200 (50 mm) Dist. B10@200 (60 mm)	393 mm <sup>2</sup>	OK
Leverarm $z=fn(d,b,As,f_y,F_{cu})$	195 mm, 1000 mm, 393 mm <sup>2</sup> , 460 N/mm <sup>2</sup> , 30 N/mm <sup>2</sup>	185 mm	
$M_r=fn(above, x, x/d)$	14 mm, 0.07	31.8 kN.m	
Moment Capacity Check (M/M <sub>r</sub> )	M 0.4 kN.m, M <sub>r</sub> 31.8 kN.m	0.013	OK
Shear Capacity Check	F 5.3 kN, $v_c$ 0.471 N/mm <sup>2</sup> , F <sub>vr</sub> 91.9 kN	0.06	OK

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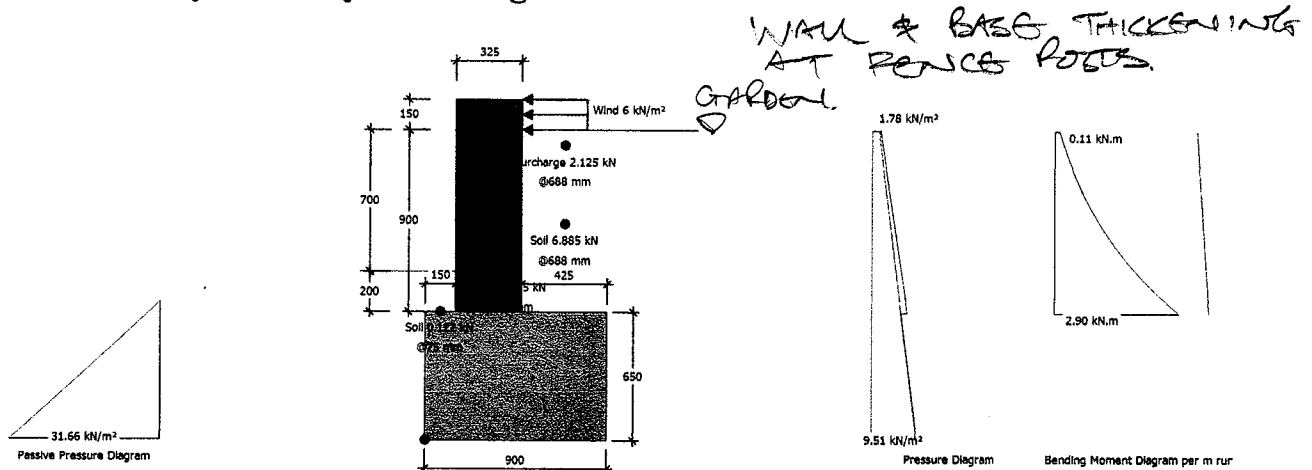
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## Boundary wall 600 Max Plus Fence

### Gravity Masonry Retaining Wall with Un-Reinforced Concrete Base

**Summary of Design Data****Notes**

Material Densities (kN/m³)

Special Assumptions (virtual back)

Concrete grade

Surcharge and Water Table

Unplanned excavation depth

All dimensions are in mm and all forces are per metre run

Soil 18.00, Concrete 24.00, Masonry 20.00

No surcharge over heel

fcu 30 N/mm², Permissible tensile stress 0.250 N/mm²

Surcharge 5.00 kN/m², Fully drained

Front of wall 155 mm

**Soil Properties**

Bearing pressure

Back Soil Friction and Cohesion

Base Friction and Cohesion

Front Soil Friction and Cohesion

Premissible service pressure @ front 100.00 kN/m², @ back 100.00 kN/m²

 $\alpha = \text{Atn}(\tan(33)/1.2) = 28.42^\circ$  $\delta = \text{Atn}(0.75 \times \tan(\text{Atn}(\tan(33)/1.2))) = 22.09^\circ$  $\phi = \text{Atn}(\tan(30)/1.2) = 25.69^\circ$ **Loading Cases** $G_{\text{Soil}}$ - Soil Self Weight,  $G_{\text{Wall}}$ - Wall & Base Self Weight,  $F_{\text{VHeel}}$ - Vertical Loads over Heel, $P_a$ - Active Earth Pressure,  $P_{\text{surcharge}}$ - Earth pressure from surcharge,  $P_p$ - Passive Earth Pressure

Case 1: Geotechnical Design

 $1.00 G_{\text{Soil}} + 1.00 G_{\text{Wall}} + 1.00 F_{\text{VHeel}} + 1.00 P_a + 1.00 P_{\text{surcharge}} + 1.00 P_p$ 

Case 2: Structural Ultimate Design

 $1.40 G_{\text{Soil}} + 1.40 G_{\text{Wall}} + 1.60 F_{\text{VHeel}} + 1.00 P_a + 1.00 P_{\text{surcharge}} + 1.00 P_p$ **Geotechnical Design****Wall Stability - Virtual Back Pressure**

Case 1 Overturning/Stabilising 5.016/11.734

0.427 OK

**Wall Sliding - Virtual Back Pressure** $F_x / (R_x \text{Friction} + R_x \text{Passive})$  8.558/(11.313+10.118)

0.399 OK

**Soil Pressure**

Virtual Back 73.346/100 kN/m², Length under pressure 0.818 m

0.733 OK

Wall Back (No uplift)

Max(59.285/100, 7.377/100) kN/m²

0.593 OK

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**Structural Design****Masonry Wall Details**

Partial Safety Factor ( $\gamma_{mc}/\gamma_{mf}$ )	Units Category II, Execution Control Class 2	3/2.7	Table NA.1
Material	Clay bricks with water absorption between 7% and 12%		
Units and Mortar Strength	5 N/mm <sup>2</sup> . Mortar designation M12/(i)		
Compressive Strength ( $f_k$ )	Group 1, $\gamma=20$ kN/m <sup>3</sup>	2.5 N/mm <sup>2</sup>	Table NA.4

**Wall Design (Inner Face Tension)**

Critical Section	Critical @ 0 mm from base, Case 2		
Section Properties @ Base	$t=325$ mm, Area=3250 cm <sup>2</sup> , $Z_b=17604$ cm <sup>3</sup>		
Flexural Strength $f_{xkl}$	$f_{xkl}=0.5$ , $gd=0.021$ N/mm <sup>2</sup> , $f_{xkl}=f_{xkl}+0.9$ gd. $\gamma_{mf}$	0.551 N/mm <sup>2</sup>	Table NA.6
$M_r=f_{xkl} \cdot Z_b/\gamma_{mf}$	$0.551 \times 17604/2.7$	3.59 kN.m	
Moment Capacity Check (M/M <sub>r</sub> )	M 2.9 kN.m, M <sub>r</sub> 3.6 kN.m	0.806	OK
Shear Capacity Check	F 5.6 kN, $f_{vk}0.308$ N/mm <sup>2</sup> , F <sub>vr</sub> 40.1 kN	0.14	OK

**Base Top Face Tension**

Maximum Tensile Stress	M 2.236, h 650, fcu 30, Permissible 0.25 N/mm <sup>2</sup>	0.03 N/mm <sup>2</sup>	OK
Shear Capacity Check	F 8.6 kN, vc 0.350 N/mm <sup>2</sup> , F <sub>vr</sub> 113.8 kN	0.08	OK

**Base Bottom Face Tension**

Maximum Tensile Stress	M 0.554, h 650, fcu 30, Permissible 0.25 N/mm <sup>2</sup>	0.01 N/mm <sup>2</sup>	OK
Shear Capacity Check	F 7.2 kN, vc 0.350 N/mm <sup>2</sup> , F <sub>vr</sub> 113.8 kN	0.06	OK