
Development of land at former Wombwell High School Barnsley

Flood Risk Assessment

Client:

Premier Construction Northern
51 Rimington Road
Wombwell
Barnsley
S73 8DQ

Prepared by:

joc consultants ltd

Park Farm House
Leathley Lane
Leathley
Otley
LS21 2JU

REVISION HISTORY

Revision	Date	Details
00	11 th January 2019	First issue
01	28 th January 2020	Amended Location Plan and Site Layout Plan

APENDICES

- A: Location Plan
- B: Topographical survey plan
- C: Planning Layout Plan
- D: Fluvial flood map
- E: Surface water flood map
- F: Reservoirs flood map
- G: REFH results
- H: Report of infiltration tests – Eastwood and Partners

ABBREVIATIONS

AEP: Annual exceedance probability

AOD: Above Ordnance Datum

CCA: Climate change allowance

E: East

FEH: Flood Estimation Handbook

FRA: Flood risk assessment

NE: North east

PPG: Planning Practice Guidance

SE: South east

SFRA: Strategic Flood Risk Assessment

ReFH2: Revitalised Flood Hydrograph model, version 2

SITE	Land at former Wombwell High School, Lundhill Road, Wombwell, Barnsley, S73 0RA.
PURPOSE OF THIS REPORT	This site-specific flood risk assessment is required in connection with a planning application to Barnsley Metropolitan Borough Council for residential development of the site.
SITE LOCATION AND DESCRIPTION	See Location Plan in Appendix A.
National Grid Reference	440295E, 402435N approx
Gross Site Area	Approximately 6.76 ha
Ground surface	100% pervious surface.
Topography	Ground levels fall towards the northern apex of the site in the range 74.7m to 50.03m AOD. See topographical survey plan in Appendix B.
Geology	<u>Superficial</u> : None recorded. <u>Bedrock</u> : Oaks Rock - Sandstone.
Watercourses	None within the vicinity of the site. The site is not within 20m of a Main River.
Reservoirs and Canals	No reservoirs within the vicinity of the site. Elsescar Canal (disused) passes around the SE, E and NE sides of the site and is approximately 220m from the site at its nearest point.
Existing site drainage	There is no evidence of an existing drainage system on the topographical survey plan.
Existing sewers	It is not known whether there are any sewers crossing the site.
THE DEVELOPMENT	A development of 235 dwellings is proposed as shown on the Site Layout Plan in Appendix C. Access to the site will be off Lundhill Road, as shown on the site layout plan.

VULNERABILITY CLASSIFICATION	The development is classified as 'More Vulnerable' , in accordance with Table 2 of the Planning Practice Guidance for Flood Risk and Coastal Change, paragraph 066.
FLOOD ZONE	Flood zone 1, (see Appendix D). <u>Reference:</u> Flood Map for Planning.
REQUIREMENT TO CONSULT THE ENVIRONMENT AGENCY	Not required when the development is in flood zone 1 and not within 20m of a main river or in a critical drainage area. <u>Reference:</u> Environment Agency Standing Advice.
THE SEQUENTIAL TEST	The Sequential Test is not required as the development is in Flood Zone 1.
REQUIREMENT FOR THE EXCEPTION TEST	Not required as the development is in Flood Zone 1. <u>Reference:</u> Planning Practice Guidance for Flood Risk and Coastal Change, paragraph 067.
HISTORY OF FLOODING	There is no available evidence of historic or potential flooding of the site.
FLUVIAL FLOODING	
Functional floodplain	The site is not in the functional floodplain.
Annual probability of fluvial flooding	Less than 0.1%.
Flood defences	None
Loss of floodplain storage	None
Obstruction to overland flow routes	None
Flood warning area	The site is not in a Flood Warning Area

SURFACE WATER FLOODING

Risk of surface water flooding

The Updated Surface Water Flood Map indicates a very low risk with no depths indicated.

See Appendix E.

Critical Drainage Areas

The site is not in a critical drainage area.

GROUNDWATER FLOODING

Groundwater flooding occurs when the water table rises above the ground surface or enters basements. It is typically associated with highly permeable rock such as chalk and highly fissured limestone. These geological conditions are not present at the site and the risk of this type of flooding at the site is therefore assessed to be very low.

SEWER FLOODING

The site in its existing condition is not at risk from sewer flooding. Following development, sewer flooding could occur if the capacity of the sewers is exceeded, but the risk of such flooding is assessed to be low.

FLOODING FROM RESERVOIRS AND CANALS

The site is not in an area at risk of flooding from reservoirs or canals.

See Appendix F.

EFFECT OF THE DEVELOPMENT ON FLOOD RISK

Fluvial and tidal flood risk

No effect

Surface water flood risk

The effect of the development on surface water runoff rates and volumes has been assessed using FEH Point Data and the ReFH2 model. A summary of the results is provided in Appendix G.

The results show that the development, which is assumed for the purposes of this FRA to convert 50% of the site to impervious area, will potentially increase runoff rates and volumes by an average of 53% and 30% respectively.

Groundwater flood risk

No effect

Sewer flooding risk

No effect

EFFECT OF CLIMATE CHANGE

Climate change must be considered over the expected lifetime of the development which, for residential development is defined to be 100 years in paragraph 026 of the Planning Practice Guidance. Climate change must therefore be considered up to 2118.

Current guidance on the application of climate change allowances was issued in February 2016 and updated on 3rd February 2017. The guidance provides the anticipated changes to peak river flow and rainfall intensity for different scenarios of carbon dioxide emissions over future epochs up to 2115.

The effects of climate change on peak river flow will not affect the flood zone designation throughout the lifetime of the development as the site is not at risk from fluvial flooding.

The current guidance requires the Central and Upper End allowances to be used when assessing the effects of increases to peak rainfall intensities. The allowances apply across the whole of England and in the period 2070 to 2115 are:

- Central allowance: 20%
- Upper end allowance: 40%

The effects of these climate change allowances are shown in the summary of the ReFH2 results in Appendix G and the detailed drainage design must take into account the range of climate change effects on surface water runoff.

FLOOD RISK MANAGEMENT

Fluvial flood risk

No recommendations

Surface water flood risk

The effect of the development on surface water flood risk can be mitigated by the application of sustainable drainage principles in the detailed drainage design of the drainage system.

Peak flow control

The underlying geology of the site suggests that infiltration drainage could be feasible. Infiltration tests were carried by Eastwood and Partners in December 2018 and their report is provided in Appendix H.

The report concludes that infiltration drainage will be feasible in the areas of sand and gravel, but where reworked clay is present the infiltration rates were poor.

Attenuation storage

Attenuation storage will be required to accommodate the excess runoff volume from the critical duration event. The form and capacity of this storage will be determined in the detailed design of the drainage system for the development.

As a preliminary estimate, the required storage capacity, should surface water be discharged to a sewer, is estimated to be:

- 1% AEP with 20% CCA: 2,072m³
- 1% AEP with 40% CCA: 2,527m³

The actual storage capacity will need to be verified in the detailed drainage design.

In the event that infiltration drainage is proposed, the storage capacity will depend on the infiltration rate determined in field tests.

Groundwater flood risk

No recommendations.

Sewer flooding risk

No recommendations.

Reservoir flood risk

No recommendations.

CONCLUSIONS

1. The development classification is **More Vulnerable**.
2. The site is in flood zone 1 where the annual probability of fluvial flooding is less than 0.1%.
3. There is no requirement for the Environment Agency to be consulted on this development.
4. There is no requirement for the Sequential Test or the Exception Test as the proposed development is in Flood Zone 1.
5. There is no evidence of historic flooding at the site.
6. The risk of surface water flooding is very low.
7. The risk of groundwater flooding is assessed to be low.
8. The risk of sewer flooding is assessed to be low.
9. The site is not in an area at risk of flooding from reservoirs or canals.
10. The development will increase peak surface water runoff rates by approximately 53% and peak surface water runoff volume by approximately 30%.

The effect of the development can be mitigated by the application of sustainable drainage principles, limiting the runoff rate and providing attenuation storage for the excess runoff volume.
11. The geology underlying the site suggests that infiltration drainage could be feasible and infiltration tests have confirmed this in the areas where there is sand and gravel.

RECOMMENDATIONS

1. It is recommended that a detailed drainage design is prepared and submitted to Barnsley MDC and Yorkshire Water for approval, prior to construction.

USE OF REPORT

This report is prepared specifically for Premier Construction Northern for the purpose of the aforementioned planning application and the report may not be used for any other purpose and it may not be assigned to any third party without our written permission.

DISCLAIMER

This flood risk assessment is based on data available at the time of its preparation and JOC Consultants Ltd accepts no liability for the consequences of any changes to or re-assessment of this data in the future.

APPENDIX A

Location Plan

Former Wombwell High School Site, off Lundhill Road, Wombwell, S70 0RA



Figure 1: Location Plan

APPENDIX B

Topographical Survey Plan

APPENDIX C

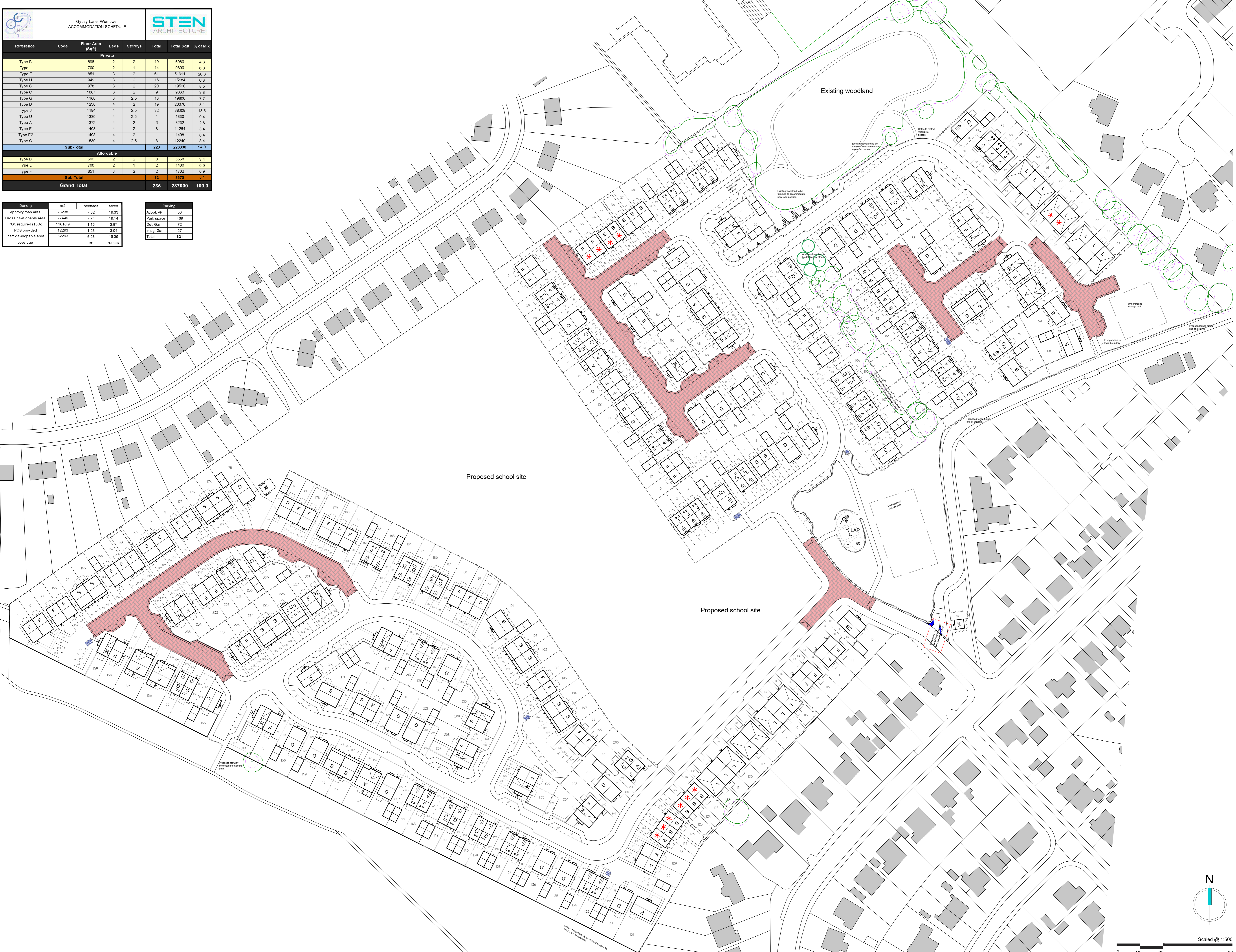
Planning Layout Plan

Drawing No: 1876.01 revision W

Reference	Code	Floor Area (sqm)	Beds	Storeys	Total	Total Sqft	% of Mix
Private							
Type B	696	2	2	10	6960	4.3	
Type L	700	2	1	14	9800	6.0	
Type F	851	3	2	61	51911	26.0	
Type H	949	3	2	16	15184	6.8	
Type S	918	3	2	20	19500	8.5	
Type C	1007	3	2	9	9063	3.8	
Type G	1100	3	2.5	18	19800	7.7	
Type D	1230	4	2	19	23370	8.1	
Type J	1194	4	2.5	32	38208	13.6	
Type U	1330	4	2.5	1	1330	0.4	
Type A	1372	4	2	6	8232	2.8	
Type E	1408	4	2	8	11264	3.4	
Type E2	1408	4	2	1	1408	0.4	
Type Q	1530	4	2.5	8	12240	3.4	
Sub-Total				223	228330	94.9	
Affordable							
Type D	696	2	2	9	5568	3.4	
Type L	700	2	1	2	1400	0.9	
Type F	851	3	2	2	1702	0.9	
Sub-Total				12	8670	5.1	
Grand Total				235	237000	100.0	

Density	m2	hectares	acres
Approx gross area	76238	7.82	19.33
Gross developable area	72448	7.74	19.14
POS required (15%)	11616.9	1.16	2.87
POS provided	12293	1.23	3.04
nett developable area coverage	62293	6.23	15.39
		38	15398

Parking	
Adopt VP	53
Dark space	409
Det Car	72
Integ. Car	27
Total	621



Notes:
 This drawing design and concepts are copyright of STEN Architecture.
 All Dimensions are to be verified on site before any work commences. If any discrepancies, errors or omissions are noted, these are to be reported to STEN Architecture immediately.
 If any other drawings are reference within this layout, please refer to the specific detailed drawing for design, materials and specific working practices.

- PLANNING LAYOUT KEY:**
- Boundary treatments**
- 1.8m Brick wall & fence panel
 - 1.8m Brick pier and low wall railing infill
 - 1.8m Close boarded timber fence
 - 1.5m Hit & Miss fence
 - 0.9m Metal railings
 - 0.45m Knee rail
- General**
- Affordable plot
 - Bin collection point (bin collection day only)
 - Site boundary
 - Herringbone Block paving
 - Retained tree
 - Proposed drainage easement
 - Incidental parking space.

W	Layout updated to planning office and highway officer comments.	TS	27.01.20
V	Rumble strips removed from build outs.	TS	23.01.20
U	Layout updated to Highways and planning officers comments.	TS	16.01.20
T	Bottom parcel redesign to show no development of Gypsy Lane Junction and new connection to Gypsy Lane shown on layout. Schedule and plot numbers updated to suit.	TS	17.12.19
S	Boundary enclosures shown to be 2m away from vehicle reversing manoeuvres. Speed humps shown as required. Incidental parking spaces shown. Proposed works to Gypsy Lane shown.	TS	05.12.19
R	Site entrance reverted back to Revision N.	TS	04.10.19
Q	Alignment of Gypsy Lane amended. Bollard role amended. Road amended by plots 233-238 to accommodate via split.	BMS	12.08.19
P	Site entrance, turning head off gypsy lane moved to accommodate highway comments, raised table adjacent POS.	TS	04.09.19
N	Plots 115-131 replanned to clients comments. Overall number reduced to 238 as a result.	TS	29.08.19
M	Adoptable surfaces adjacent plots 51, 55, 80, 85, 91, 105, 106, 163, 235 & 239 to accommodate forward visibility and visibility splays. Plots 15, 50-57, 44, 53, 103-104 & 233-239, along with associated parking and garages, moved to suit.	TS	07.08.19
L	Turning head to Gypsy lane extended.	TS	07.08.19
K	Forward visibility and visibility splays plotted on layout. Plots 1-14 & 233-239 repositioned to suit. Highways extended to incorporate visibility where applicable. Metal railing heights reduced.	TS	29.07.19
J	Junction adjacent plots 163/239 amended. Plots 74/75 retained to A type, schedule updated.	TS	26.07.19
H	Overall site reduced to 240.	TS	25.07.19
G	Overall site reduced to 240.	TS	25.07.19
F	Upper parcel of development redesigned in line with LPA comments. School repositioned and development row included within north-west parcel.	TS	23.07.19
E	Amendments to layout based on feedback from the local authority.	NJ	31.05.19
D	Visibility splays indicated on layout. Footpath adjacent plot 73 amended to suit. Plot 216/218 replanned to accommodate forward visibility. Site entrance radius reduced to 6m.	TS	23.04.19
C	LPA and associated footpath connections updated to landscaped proposals. Position of Eastern storage tank moved to engineers details. House types G & U introduced. General plot amends to clients comments.	TS	06.03.19
B	Developable areas amended in line with latest revision.	TS	27.02.19
A	Affordable contribution amended to include 4 x 3 bed units as requested by LPA.	TS	14.01.19
REV.	DESCRIPTION	BY:	DATE

STEN ARCHITECTURE
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 LinkedIn: Sten Architecture

CLIENT: Premier construction northern
 51 Rimington Road
 Wombwell
 Barnsley
 S73 8DQ

SITE: Wombwell

TITLE: Planning Layout

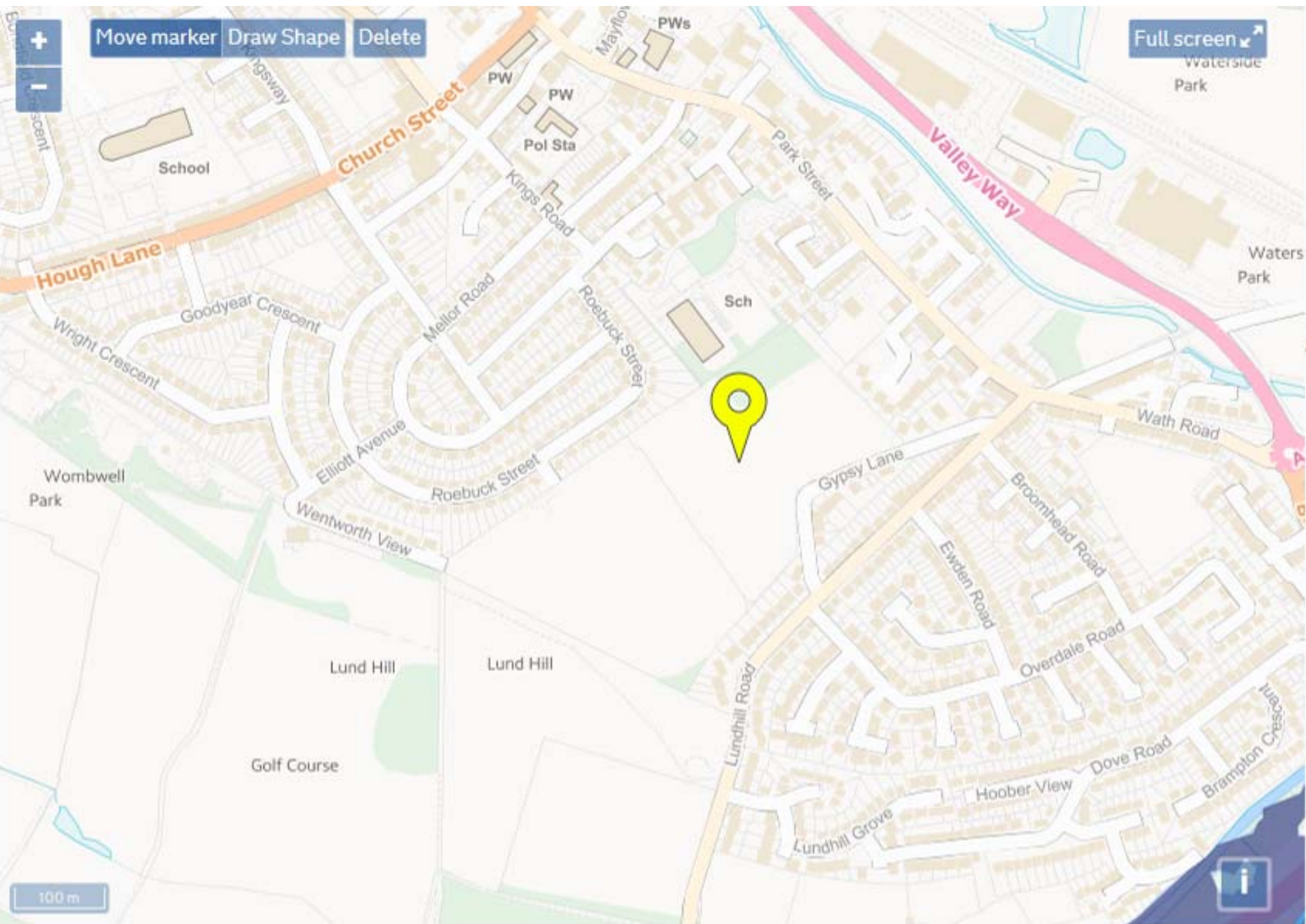
SCALE AT A0: 1:500 DATE: 13.12.18 DRAWN: TS CHECKED: BS

PROJECT NO: 1876 DRAWING NO: 1876.01 REVISION: W

Scaled @ 1:500
 0 10m 20m 50m

APPENDIX D

Fluvial flood map



+ Move marker Draw Shape Delete
-

Full screen ↗
Waterside Park



Selected location



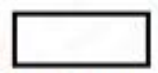
Flood zone 3



Areas benefiting from flood defences



Flood zone 2



Flood zone 1



Flood defence



Main river



Flood storage area

100 m



APPENDIX E

Surface water flood map



Flood risk from rivers or the sea

- Extent of flooding
- Depth and flow estimates at monitoring stations



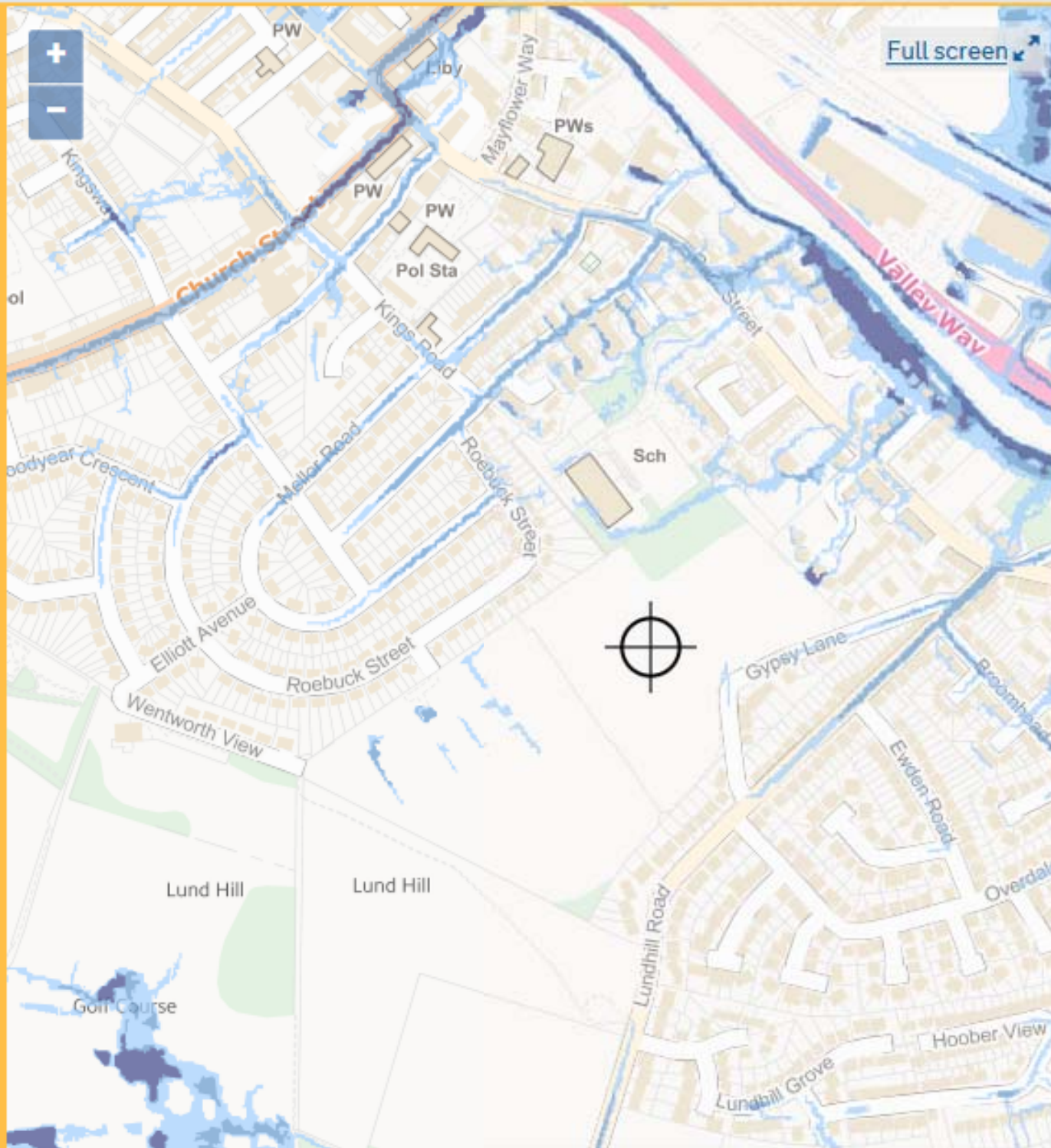
Flood risk from surface water

- Extent of flooding
- High risk: depth
- High risk: velocity
- Medium risk: depth
- Medium risk: velocity
- Low risk: depth
- Low risk: velocity



Flood risk from reservoirs

- Extent of flooding
- Flood depth



Flood risk



High



Medium



Low




Very low




Location you selected

APPENDIX F


Reservoirs flood map

 Flood risk from rivers or the sea

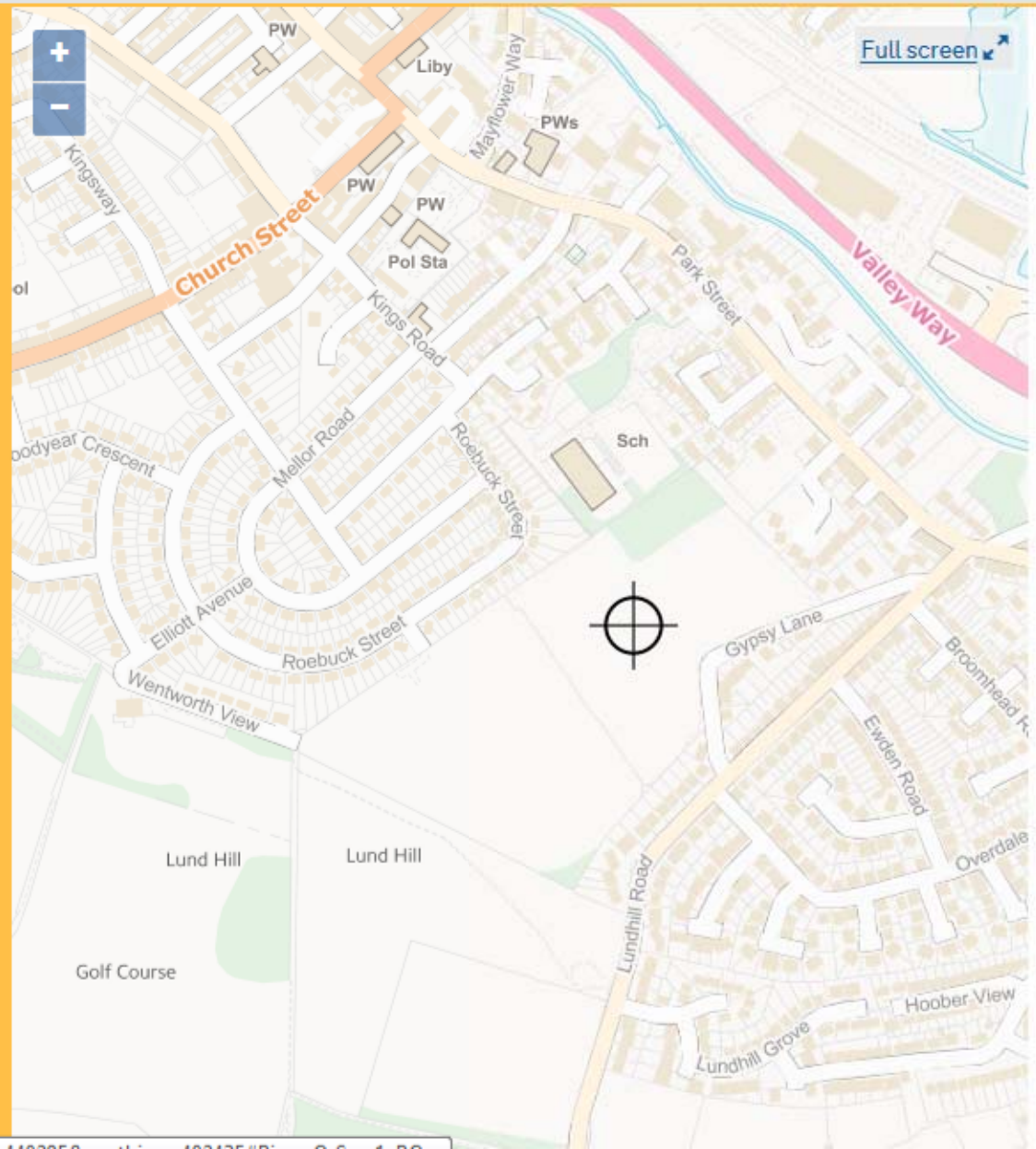
- Extent of flooding
- Depth and flow estimates at monitoring stations

 Flood risk from surface water

- Extent of flooding
- High risk: depth
- High risk: velocity
- Medium risk: depth
- Medium risk: velocity
- Low risk: depth
- Low risk: velocity

 Flood risk from reservoirs

- Extent of flooding
- Flood depth



Flood risk



Maximum extent of flooding



Location you selected

APPENDIX G

REFH2 Results

19/003: Wombwell High School Site

SUMMARY OF REFH RESULTS

Event AEP	Greenfield		Brownfield		Post development		% change	
	Peak Flow l/s	Volume m ³	Peak Flow l/s	Volume m ³	Peak Flow l/s	Volume m ³	Peak Flow	Volume
100%	33.11	431.56			51.55	574.53	56%	33%
50%	37.59	496.38			58.57	658.80	56%	33%
3.3%	86.05	1,197.46			131.28	1,542.09	53%	29%
1%	119.25	1,678.73			178.28	2,122.81	50%	26%
						Average:	53%	30%
1% - 20% CCA					214.06	2568.77		
1% - 40% CCA					250.59	3023.35		
Estimate of attenuation storage required:					20% CCA	2072.39		
					40% CCA	2526.97		

UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:04:58 AM by John
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

Site details

Checksum: 1DB7-59BB

Site name: Wombwell High School Site - Greenfield
Easting: 440289
Northing: 402467
Country: England, Wales or Northern Ireland
Catchment Area (km²): 0.07
Using plot scale calculations: Yes
Site description: Greenfield

Model run: 1 year

Summary of results

Rainfall - FEH 2013 (mm):	16.95	Total runoff (ML):	0.43	431.56 m ³
Total Rainfall (mm):	10.61	Total flow (ML):	0.75	
Peak Rainfall (mm):	3.59	Peak flow (m ³ /s):	0.03	33.11 l/s

Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

* Indicates that the user locked the duration/timestep

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m ³ /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km ²)	0	No
Urbext 2000	0	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Sewered area (km ²)	0.00	Yes
Sewer capacity (m ³ /s)	0.00	Yes

UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:05:33 AM by John
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Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

Site details

Checksum: 1DB7-59BB

Site name: Wombwell High School Site - Greenfield
Easting: 440289
Northing: 402467
Country: England, Wales or Northern Ireland
Catchment Area (km²): 0.07
Using plot scale calculations: Yes
Site description: Greenfield

Model run: 2 year

Summary of results

Rainfall - FEH 2013 (mm):	19.40	Total runoff (ML):	0.50	496.38 m ³
Total Rainfall (mm):	12.15	Total flow (ML):	0.86	
Peak Rainfall (mm):	4.10	Peak flow (m ³ /s):	0.04	37.59 l/s

Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

* Indicates that the user locked the duration/timestep

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m ³ /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km ²)	0	No
Urbext 2000	0	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Sewered area (km ²)	0.00	Yes
Sewer capacity (m ³ /s)	0.00	Yes

UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:05:51 AM by John
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Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

Site details

Checksum: 1DB7-59BB

Site name: Wombwell High School Site - Greenfield
Easting: 440289
Northing: 402467
Country: England, Wales or Northern Ireland
Catchment Area (km²): 0.07
Using plot scale calculations: Yes
Site description: Greenfield

Model run: 30 year

Summary of results

Rainfall - FEH 2013 (mm):	44.58	Total runoff (ML):	1.20	1197.46 m ³
Total Rainfall (mm):	27.91	Total flow (ML):	2.06	
Peak Rainfall (mm):	9.43	Peak flow (m ³ /s):	0.09	86.05 l/s

Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

* Indicates that the user locked the duration/timestep

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m ³ /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km ²)	0	No
Urbext 2000	0	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Sewered area (km ²)	0.00	Yes
Sewer capacity (m ³ /s)	0.00	Yes

UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:06:18 AM by John
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Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

Site details

Checksum: 1DB7-59BB

Site name: Wombwell High School Site - Greenfield
Easting: 440289
Northing: 402467
Country: England, Wales or Northern Ireland
Catchment Area (km²): 0.07
Using plot scale calculations: Yes
Site description: Greenfield

Model run: 100 year

Summary of results

Rainfall - FEH 2013 (mm):	60.65	Total runoff (ML):	1.68	1678.73 m ³
Total Rainfall (mm):	37.97	Total flow (ML):	2.90	
Peak Rainfall (mm):	12.83	Peak flow (m ³ /s):	0.12	119.25 l/s

Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

* Indicates that the user locked the duration/timestep

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m ³ /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km ²)	0	No
Urbext 2000	0	No
Impervious runoff factor	0.7	No
Imperviousness factor	0.3	No
Tp scaling factor	0.5	No
Sewered area (km ²)	0.00	Yes
Sewer capacity (m ³ /s)	0.00	Yes

UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:08:03 AM by John
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

Site details

Checksum: AFED-CF4C

Site name: Wombwell High School Site
Easting: 440289
Northing: 402467
Country: England, Wales or Northern Ireland
Catchment Area (km²): 0.07
Using plot scale calculations: Yes
Site description: Post development

Model run: 1 year

Summary of results

Rainfall - FEH 2013 (mm):	16.95	Total runoff (ML):	0.57	574.53 m ³
Total Rainfall (mm):	10.61	Total flow (ML):	0.73	
Peak Rainfall (mm):	3.59	Peak flow (m ³ /s):	0.05	51.55 l/s

Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

* Indicates that the user locked the duration/timestep

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m ³ /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km ²)	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km ²)	0.00	Yes
Sewer capacity (m ³ /s)	0.00	Yes

UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:08:46 AM by John
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

Site details

Checksum: AFED-CF4C

Site name: Wombwell High School Site
Easting: 440289
Northing: 402467
Country: England, Wales or Northern Ireland
Catchment Area (km²): 0.07
Using plot scale calculations: Yes
Site description: Post development

Model run: 2 year

Summary of results

Rainfall - FEH 2013 (mm):	19.40	Total runoff (ML):	0.66	658.80 m ³
Total Rainfall (mm):	12.15	Total flow (ML):	0.84	
Peak Rainfall (mm):	4.10	Peak flow (m ³ /s):	0.06	58.57 l/s

Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

* Indicates that the user locked the duration/timestep

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m ³ /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km ²)	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km ²)	0.00	Yes
Sewer capacity (m ³ /s)	0.00	Yes

UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:09:05 AM by John
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

Site details

Checksum: AFED-CF4C

Site name: Wombwell High School Site
Easting: 440289
Northing: 402467
Country: England, Wales or Northern Ireland
Catchment Area (km²): 0.07
Using plot scale calculations: Yes
Site description: Post development

Model run: 30 year

Summary of results

Rainfall - FEH 2013 (mm):	44.58	Total runoff (ML):	1.54	1542.09 m ³
Total Rainfall (mm):	27.91	Total flow (ML):	1.97	
Peak Rainfall (mm):	9.43	Peak flow (m ³ /s):	0.13	131.28 l/s

Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

* Indicates that the user locked the duration/timestep

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m ³ /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km ²)	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km ²)	0.00	Yes
Sewer capacity (m ³ /s)	0.00	Yes

UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:09:31 AM by John
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

Site details

Checksum: AFED-CF4C

Site name: Wombwell High School Site
Easting: 440289
Northing: 402467
Country: England, Wales or Northern Ireland
Catchment Area (km²): 0.07
Using plot scale calculations: Yes
Site description: Post development

Model run: 100 year

Summary of results

Rainfall - FEH 2013 (mm):	60.65	Total runoff (ML):	2.12	2122.81 m ³
Total Rainfall (mm):	37.97	Total flow (ML):	2.73	
Peak Rainfall (mm):	12.83	Peak flow (m ³ /s):	0.18	178.28 l/s

Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

* Indicates that the user locked the duration/timestep

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m ³ /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km ²)	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km ²)	0.00	Yes
Sewer capacity (m ³ /s)	0.00	Yes

UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:24:45 AM by John
 Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

Site details

Checksum: 1167-CB3B

Site name: Wombwell High School Site

Easting: 440289

Northing: 402467

Country: England, Wales or Northern Ireland

Catchment Area (km²): 0.07

Using plot scale calculations: Yes

Site description: Post development: 1% AEP & 20% CCA

Model run: 200 year

Summary of results

Rainfall - FEH 2013 (mm):	72.75	Total runoff (ML):	2.57	2568.77 m ³
Total Rainfall (mm):	45.55	Total flow (ML):	3.31	
Peak Rainfall (mm):	15.39	Peak flow (m ³ /s):	0.21	214.06 l/s

Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

* Indicates that the user locked the duration/timestep

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m ³ /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km ²)	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km ²)	0.00	Yes
Sewer capacity (m ³ /s)	0.00	Yes

UK Design Flood Estimation

Generated on Friday, January 11, 2019 11:25:12 AM by John
Printed from the ReFH Flood Modelling software package, version 2.2.6589.25305

Summary of estimate using the Flood Estimation Handbook revitalised flood hydrograph method (ReFH)

Site details

Checksum: 1167-CB3B

Site name: Wombwell High School Site

Easting: 440289

Northing: 402467

Country: England, Wales or Northern Ireland

Catchment Area (km²): 0.07

Using plot scale calculations: Yes

Site description: Post development: 1% AEP & 40% CCA

Model run: 367 year

Summary of results

Rainfall - FEH 2013 (mm):	84.88	Total runoff (ML):	3.02	3023.35 m ³
Total Rainfall (mm):	53.14	Total flow (ML):	3.92	
Peak Rainfall (mm):	17.95	Peak flow (m ³ /s):	0.25	250.59 l/s

Parameters

Where the user has overridden a system-generated value, this original value is shown in square brackets after the value used.

* Indicates that the user locked the duration/timestep

Rainfall parameters (Rainfall - FEH 2013 model)

Name	Value	User-defined?
Duration (hh:mm:ss)	03:30:00	No
Timestep (hh:mm:ss)	00:30:00	No
SCF (Seasonal correction factor)	0.63	No
ARF (Areal reduction factor)	1 [0.99]	Yes
Seasonality	Winter	n/a

Loss model parameters

Name	Value	User-defined?
Cini (mm)	151.42	No
Cmax (mm)	260.56	No
Use alpha correction factor	No	No
Alpha correction factor	n/a	No

Routing model parameters

Name	Value	User-defined?
Tp (hr)	2.17 [1.24]	Yes
Up	0.65	No
Uk	0.8	No

Baseflow model parameters

Name	Value	User-defined?
BF0 (m ³ /s)	0	No
BL (hr)	30.46 [26.16]	Yes
BR	0.72	No

Urbanisation parameters

Name	Value	User-defined?
Urban area (km ²)	0.03 [0]	Yes
Urbext 2000	0.32 [0]	Yes
Impervious runoff factor	1 [0.7]	Yes
Imperviousness factor	1 [0.3]	Yes
Tp scaling factor	0.5	No
Sewered area (km ²)	0.00	Yes
Sewer capacity (m ³ /s)	0.00	Yes

APPENDIX H

Report of infiltration tests

Eastwood and Partners report dated 27th December 2018

Mr M Platts
Premier Group
51 Rimington Road
Wombwell
Barnsley
S73 8DQ

PR/AJK/SAE/43497-001

27 December 2018

Dear Martyn,

Wombwell High School

We are writing to report the findings of the infiltration testing undertaken on the above site on 17 and 18 December 2018.

The site comprises a former school, now demolished, and associated playing fields. The site is split into three terraces, with the upper terrace and former school present in the west of the site, and the lowest terrace present in the east of the site. A difference in level of approximately 5 m bgl is present between each terrace.

Site Works

Nine soakaway pits were excavated across the site, to depths of between 1.2 m and 2.3 m below ground level (bgl).

Water was then pumped in to each pit to a depth of at least 500 mm, and the change in water level was monitored at regular intervals over at least a three hour period, or until the water had drained from each pit, whichever came first. Between one and three infiltration tests were undertaken in each pit.

Two trial pits were additionally excavated to 2.4 m and 3.4 m bgl, in order to assess the depth of fill in the east of the uppermost terrace.

The locations of the soakaway and trial pits are shown on the Exploratory Hole Location Plan, drawing number 43497/001/A, which is appended to this report.

Also at: - Centaur House, Ancells Business Park, Ancells Rd, Fleet GU51 2UJ Tel: 01252 360580 Fax: 01252 360581

Directors: P Richardson BSc, CEng, MICE, MIStructE S D Preston BEng, CEng, FICE, FIStructE N J Baines BSc, CEng, MICE, MCIWEM
S R Ellis BEng, CEng, MIStructE, MICE K R Pursall BEng, CEng, MIStructE
C A Topliss BSc, CEng, CSci, CGeol, SiLC, MICE, FGS S J English BEng, CEng, MIStructE A R Priest BEng
Senior Associates: K Newsome BSc, CEng, MICE, MIStructE S J Mitchell BSc, MSc, CEng, MEI, MCIBSE, MASHRAE A Allison BEng
M Young MA, CEng, MICE, MIStructE C A Wood BSc, CEng, MIStructE, MICE
Associates: K Edwards MSci, FGS A J Kerslake BEng A G Marshall BEng, CEng, MIStructE C Hodge EngTech, MICE P A Harrison BEng, CEng, MIStructE
M P Chappell BEng, IEng, AMIStructE M Dyson BSc, CEng, MIStructE

Ground Conditions

Historically, a cut and fill earthworks exercise has occurred on the site in order to create three flat terraces for the former school playing fields. Generally the surrounding land slopes from the west down to the east.

Topsoil comprising clayey sand, and occasionally sandy clay, was encountered in the excavations across the site to depths of between 0.3 m and 0.5 m bgl. This was underlain by clayey sand and gravel in SA3, SA6 and SA7, encountered to the base of the pit in SA3 and underlain by weak to medium strong sandstone at 1.1 m and 0.9 m bgl respectively in SA6 and SA7.

In the remainder of exploratory holes, made ground comprising sandy gravelly reworked clay, with occasional to frequent cobbles of sandstone with depth was encountered, with the depth of made ground increasing towards the east. This was underlain by natural sand and gravel from 0.6 m bgl in SA1 and SA4, and from 1.4 m bgl in SA7, and by weak to medium strong sandstone from depths of between 1.1 m and 2.25 m bgl in SA2, SA8, SA9, TP1 and TP2. Pits excavated in the west of each terrace generally recorded sandstone bedrock at shallower depth than those in the east of each terrace.

The trial pit and soakaway logs are appended to this report.

Infiltration Results

The results and calculation of Infiltration Results are appended to this report, and are summarised in the table below:

Soakaway	Test Material	BRE365 Soil Infiltration Rate (x10-6) m/s	Average Infiltration Rate
SA1 Test 1	Reworked clay over sand and gravel	34	31
SA1 Test 2		69	56
SA1 Test 3		47	57
SA2	Reworked clay over sandstone at base	0	0
SA3 Test 1	Sand and gravel	360	580
SA3 Test 2		240	360
SA3 Test 3		310	430
SA4 Test 1	Reworked clay over sand and gravel	21	34
SA4 Test 2		25	40
SA5 Test 1	Reworked clay over sand and gravel	45	66
SA5 Test 2		18	33
SA6 Test 1	Sand and gravel over sandstone	220	310
SA6 Test 2		120	180
SA6 Test 3		120	160

SA7 Test 1	Gravel over sandstone	33	39
SA7 Test 2		17	25
SA8	Reworked clay over sandstone	-	2.5
SA9 Test 1	Reworked clay over sandstone	98	98
SA9 Test 2		64	76
SA9 Test 3		61	79

Conclusion

Soakaways excavated within sand and gravel generally performed the best, with those soakaways whose pit walls generally comprised reworked clay performing the worst overall.

Therefore it is recommended soakaways be constructed within the sand and gravel generally found to the west of each terrace, and avoid the made ground, found to extend to significant depth towards the east of each terrace.

We trust that this meets with your approval, however if you have any comments or queries please do not hesitate to contact us.

Yours sincerely






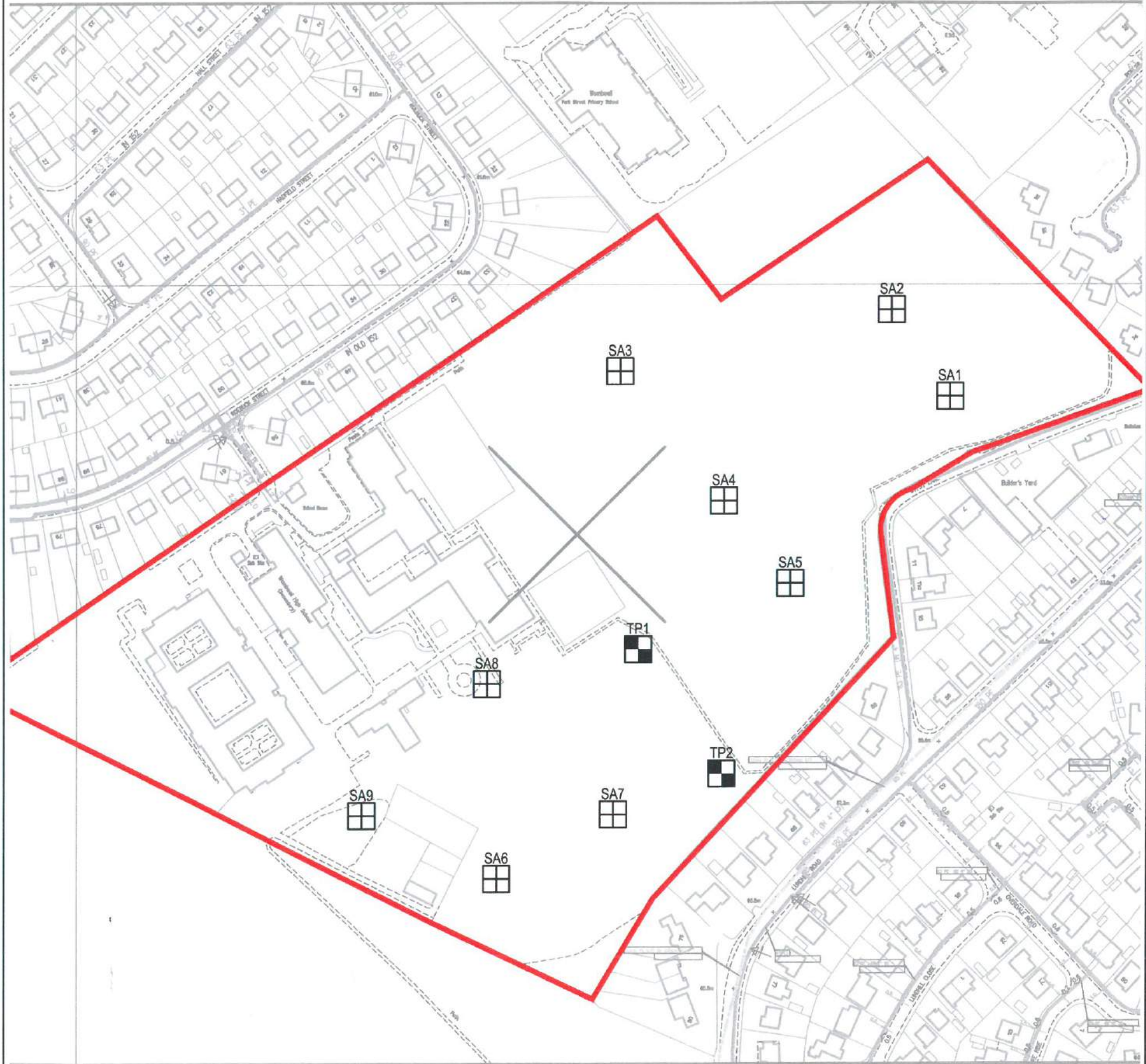
Andrew Kerlake
Associate

- Enc. Exploratory Hole Plan
- Infiltration Results - SA1 to SA9
- Trial Pit and Soakaway Logs

INFORMATION WITHIN THIS DRAWING IS NOT NECESSARILY PRODUCED TO SCALE.
ALWAYS USE FIGURED DIMENSIONS AND CO-ORDINATES - IF IN DOUBT, ASK.

KEY:

-  Approximate location of trial pits excavated by Eastwood and Partners on 18.12.18.
-  Approximate location of soakaway excavated by Eastwood and Partners between 17.12.18 and 18.12.18.
-  Site Boundary



A	First Issue.			
REV	DESCRIPTION	SIG	CHK	DATE

**PREMIER CONSTRUCTION
NORTHERN LTD**

**WOMBWELL HIGH SCHOOL, GYPSY
LANE, WOMBWELL**

EXPLORATORY HOLE LOCATION PLAN

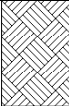

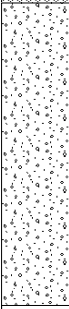
Eastwood & Partners 
CONSULTING ENGINEERS

St. Andrew's House
23 Kingfield Road
Sheffield S11 9AS
Tel 0114 255 4554 Fax 0114 255 4330
mail@eastwoodandpartners.com www.eastwoodandpartners.com

SCALE WHEN PLOTTED AT A3 1:2000			DRAWING STATUS INFORMATION	
DRAWN	CHECKED	DATE	DRAWING NUMBER	REV
TC	?	19.12.18	43497/001	A

This plan shows those pipes owned by Cadent Gas Ltd in their role as a

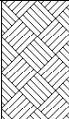
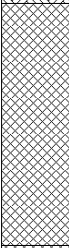
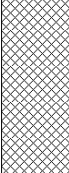
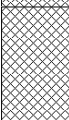

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Location:		Dimensions: 2.50m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.60m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.35			TOPSOIL: Grass over dark brown sandy CLAY.
			0.60			MADE GROUND: Light brown /orange brown sandy reworked CLAY.
			1.60			Brown Clayey SAND and GRAVEL with occasional to frequent cobbles. Gravel is fine to coarse angular to sub-angular of sandstone.
						Trialpit Complete at 1.600m

Remarks:

Stability:

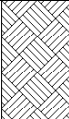
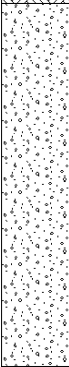
Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 2.90m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 2.25m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.40			TOPSOIL: Gras cover dark brown clayey SAND.
			1.20			MADE GROUND: Firm brown sandy reworked CLAY.
			1.80			MADE GROUND: Stiff to friable brown mottled grey sandy gravelly reworked CLAY with occasional cobbles. Gravel is medium to coarse angular to sub-angular of sandstone.
			2.20			MADE GROUND: Grey brown friable sandyreworked CLAY.
			2.25			Strong brown SANDSTONE.
Trialpit Complete at 2.250m						

Remarks:

Stability:



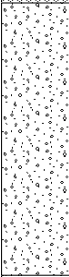
Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 2.90m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.60m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.40			TOPSOIL: Grass over dark brown clayey SAND.
			1.60			Orange brown clayey SAND and GRAVEL. Gravel is medium to coarse angular to sub-angular of sandstone. Occasional becoming frequent cobbles with depth.
						Trialpit Complete at 1.600m

Remarks:

Stability:


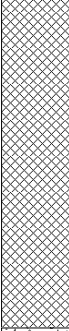
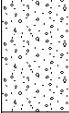
Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 3.10m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.50m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.30			TOPSOIL: Grass over dark brown clayey SAND.
			0.60			MADE GROUND: Brown very sandy reworked CLAY.
			1.50			Orange brown clayey SAND and GRAVEL. Gravel is fine to coarse subangular of sandstone. Occasional becoming frequent cobbles from 0.9 m bgl.
						Trialpit Complete at 1.500m

Remarks:

Stability:


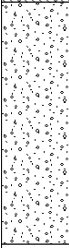

Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 2.80m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.80m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.30			TOPSOIL: Grass over dark brown clayey SAND.
			1.40			MADE GROUND: Brown sandy gravelly reworked CLAY with occasional cobbles. Gravel is fine to coarse sub-angular of sandstone.
			1.80			Brown slightly clayey SAND and GRAVEL. Gravel is fine to coarse sub-angular of sandstone, with occasional cobbles.
Trialpit Complete at 1.800m						

Remarks:

Stability:

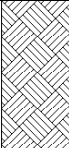
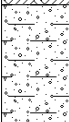
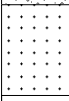
Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 3.00m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.30m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.30			TOPSOIL: Grass over dark brown clayey SAND.
			1.10			Yellow/orange brown slightly clayey SAND and GRAVEL. Gravel is fine to coarse angular to subangular of sandstone. Frequent cobbles with depth.
			1.30			Weak to medium strong yellow brown SANDSTONE recovered as cobbles and gravel.
Trialpit Complete at 1.300m						

Remarks:

Stability:

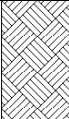

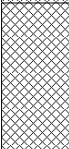

Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 3.10m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.20m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
						TOPSOIL: Grass over dark brown clayey SAND.
			0.50			Orange brown slightly clayey sandy GRAVEL. Gravel is fine to coarse angular to sub-angular of sandstone, with frequent cobbles with depth.
			0.90			Medium strong SANDSTONE recovered as sand gravel, with frequent cobbles.
			1.20			Trialpit Complete at 1.200m

Remarks:

Stability:

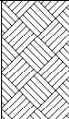

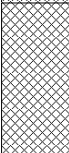

Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: 3.20m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 1.30m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
						TOPSOIL: Grass over dark brown clayey SAND.
			0.40			MADE GROUND: Brown sandy gravelly reworked CLAY. Gravel is fine to medium sub-angular of sandstone.
			0.60			POSSIBLE MADE GROUND: Yellow/orange brown sandy very gravelly CLAY. Gravel is fine to medium sub-angular of sandstone.
			1.10			Extremely weak to weak grey brown SANDSTONE, recovered as tabular gravel.
			1.30			Trialpit Complete at 1.300m

Remarks:

Stability:

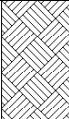
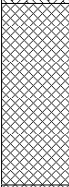

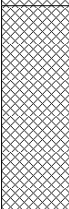
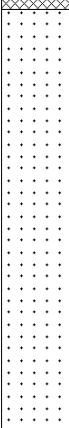
Project Name Wombwell High School		Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:			Dimensions: 3.20m	Scale 1:25
Client: Premier Construction Northern Ltd.			Depth: 1.25m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.40			TOPSOIL: Grass over dark brown clayey SAND.
			0.60			MADE GROUND: Brown sandy gravelly reworked CLAY. Gravel is fine to medium sub-angular of sandstone.
			1.10			POSSIBLE MADE GROUND: Yellowish brown sandy gravelly CLAY. Gravel is fine to coarse subangular of sandstone.
			1.25			Weak to medium strong yellow brown SANDSTONE, recovered as tabular gravel and cobbles.
Trialpit Complete at 1.250m						

Remarks:

Stability:


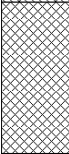
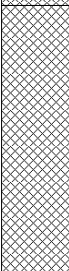

Project Name Wombwell High School	Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:		Dimensions: m	Scale 1:25
Client: Premier Construction Northern Ltd.		Depth: 3.40m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.40			TOPSOIL: Dark Brown clayey SAND.
			1.00			MADE GROUND: Brown Sandy gravelly reworked CLAY with occasional cobbles. Gravel is fine to coarse sub-angular of SANDSTONE.
			1.30			MADE GROUND: Brown sclayey gravelly SAND. Gravel is fine to coarse sub-angular of SANDSTONE with occasional cobbles.
			2.00			MADE GROUND: Brown sandy gravelly reworked CLAY with occasional cobbles. Gravel is fine to coarse sub-angular of SANDSTONE.
			3.40			Extremely weak to weak grey brown SANDSTONE recovered as sand, gravel and occasional cobbles. Cobble content increases with depth.
						Trialpit Complete at 3.400m

Remarks:

Stability:

Project Name Wombwell High School		Project No. 43497	Co-ords: - Level:	Date 19/12/2018
Location:			Dimensions: m	Scale 1:25
Client: Premier Construction Northern Ltd.			Depth: 2.40m	Logged

Samples & In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description
Depth (m)	Type	Results				
			0.30			TOPSOIL: Dark brown clayey SAND.
			0.80			MADE GROUND: Brown sandy gravelly reworked CLAY. Gravel is fine to coarse sub-angular of SANDSTONE.
			1.20			MADE GROUND: Brown sandy gravelly reworked CLAY. Gravel is fine to coarse sub-angular of SANDSTONE.
			2.10			MADE GROUND: Brown sandy gravelly reworked CLAY. Gravel is sub-angular of SANDSTONE.
			2.40			Medium strong brown SANDSTONE recovered as sand, gravel and cobbles.
Trialpit Complete at 2.400m						

Remarks:

Stability:

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA1 - Test 1

Soil Infiltration Rate in Accordance with BR365

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

V_{p75-25}

Initial parameters

Depth to water = **1040 mm** Average water depth: **280 mm**

Start time = a_{p50} **0 min** Change in water depth: **560 mm**

Final parameters

Depth to water = t_{p75-25} **600 mm** Time interval: **140 min**

End time = **140 min**

Effective Storage Volume of Water in the Trial Pit = **0.75 m³**
 75% Effective Depth = **1225 mm** from ground level
 25% Effective Depth = **1475 mm** from ground level
 Time at 75% Effective Depth = **4 minutes**
 Time at 25% Effective Depth = **64 minutes**

= **0.38 m³**

= **3.05 m²**

= **3600 sec**

= **3.4E-05 m/sec**

Average Soakaway Rate = **1.0E-04 m³/sec**

Average soakaway area = **3.24 m²** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$ **Soil Infiltration Rate = 3.4E-05 m/sec**
Average Infiltration Rate = 3.1E-05 m/sec

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA1 - Test 2

Soil Infiltration Rate in Accordance with BR365

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

V_{p75-25}

Initial parameters

Depth to water = **930** mm Average water depth: **235** mm

Start time = a_{p50} **0** min

Change in water depth: **470** mm

Final parameters

Depth to water = t_{p75-25} **400** mm Time interval: **71** min

End time = **71** min

Effective Storage Volume of Water in the Trial Pit = **0.615** m³
 75% Effective Depth = **1093** mm from ground level
 25% Effective Depth = **1298** mm from ground level
 Time at 75% Effective Depth = **3** minutes
 Time at 25% Effective Depth = **30** minutes

= **0.31** m³

= **2.77** m²

= **1620** sec

= **6.9E-05** m/sec

Average Soakaway Rate = **1.7E-04** m³/sec

Average soakaway area = **2.96** m² (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$ **Soil Infiltration Rate** = **6.9E-05** m/sec
Average Infiltration Rate = **5.6E-05** m/sec

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA1 - Test 3

Soil Infiltration Rate in Accordance with BR365

Where: V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **900 mm** Average water depth: **250 mm**

Start time = a_{p50} **0 min** Change in water depth: **500 mm**

Final parameters

Depth to water = t_{p75-25} **400 mm** Time interval: **72 min**

End time = **72 min**

Effective Storage Volume of Water in the Trial Pit = **0.66 m³**
 75% Effective Depth = **1070 mm** from ground level
 25% Effective Depth = **1290 mm** from ground level
 Time at 75% Effective Depth = **4 minutes**
 Time at 25% Effective Depth = **45 minutes**

= **0.33 m³**

= **2.86 m²**

= **2460 sec**

= **4.7E-05 m/sec**

Average Soakaway Rate = **1.7E-04 m³/sec**

Average soakaway area = **3.05 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 4.7E-05 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **average Infiltration Rate = 5.7E-05 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA2 - Test 1

Soil Infiltration Rate in Accordance with BR365

Where:

V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **1770 mm** Average water depth: **480 mm**

Start time = a_{p50} **0 min** Change in water depth: **0 mm**

Final parameters

Depth to water = t_{p75-25} **770 mm** Time interval: **243 min**

End time = **243 min**

Effective Storage Volume of Water in the Trial Pit = **0.8352 m³**
 75% Effective Depth = **1890 mm** from ground level
 25% Effective Depth = **2130 mm** from ground level
 Time at 75% Effective Depth = **N/A** minutes
 Time at 25% Effective Depth = **N/A** minutes

= **0.42 m³**

= **3.42 m²**

= **0 sec**

= **N/A m/sec**

Average Soakaway Rate = **0.0E+00 m³/sec**

Average soakaway area = **5.10 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **5 Soil Infiltration Rate = 0.0E+00 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **verage Infiltration Rate = 0.0E+00 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA3 - Test 1

Soil Infiltration Rate in Accordance with BR365

Where: V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **1130 mm** Average water depth: **235 mm**

Start time = a_{p50} **0 min** Change in water depth: **470 mm**

Final parameters

Depth to water = t_{p75-25} **600 mm** Time interval: **7 min**

End time = **7 min**

Effective Storage Volume of Water in the Trial Pit = **0.6612 m³**
 75% Effective Depth = **1315 mm** from ground level
 25% Effective Depth = **1505 mm** from ground level
 Time at 75% Effective Depth = **2 minutes**
 Time at 25% Effective Depth = **5 minutes**

= **0.33 m³**

= **3.07 m²**

= **300 sec**

= **3.6E-04 m/sec**

Average Soakaway Rate = **1.9E-03 m³/sec**

Average soakaway area = **3.39 m²** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$ **Soil Infiltration Rate = 3.6E-04 m/sec**
Average Infiltration Rate = 5.8E-04 m/sec

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA3 - Test 2

Soil Infiltration Rate in Accordance with BR365

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

V_{p75-25}

Initial parameters

Depth to water = **1130 mm** Average water depth: **225 mm**

Start time = a_{p50} **0 min** Change in water depth: **450 mm**

Final parameters

Depth to water = t_{p75-25} **580 mm** Time interval: **11 min**

End time = **11 min**

Effective Storage Volume of Water in the Trial Pit = **0.6786 m³**
 75% Effective Depth = **1288 mm** from ground level
 25% Effective Depth = **1483 mm** from ground level
 Time at 75% Effective Depth = **3.5 minutes**
 Time at 25% Effective Depth = **7.5 minutes**

= **0.34 m³**

= **3.11 m²**

= **450 sec**

= **2.4E-04 m/sec**

Average Soakaway Rate = **1.2E-03 m³/sec**

Average soakaway area = **3.32 m² (sides + base)**

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 2.4E-04 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **average Infiltration Rate = 3.6E-04 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA3 - Test 3

Soil Infiltration Rate in Accordance with BR365

Where:

V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **1020 mm**
Start time = a_{p50} **1 min**

Average water depth: **265 mm**

Change in water depth: **530 mm**

Final parameters

Depth to water = t_{p75-25} **550 mm**
End time = **11 min**

Time interval: **10 min**

Effective Storage Volume of Water in the Trial Pit = **0.9222 m³**
75% Effective Depth = **1153 mm** from ground level
25% Effective Depth = **1418 mm** from ground level
Time at 75% Effective Depth = **2 minutes**
Time at 25% Effective Depth = **7 minutes**

= **0.46 m³**

= **3.60 m²**

= **420 sec**

= **3.1E-04 m/sec**

Average Soakaway Rate = **1.5E-03 m³/sec**
Average soakaway area = **3.60 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 3.1E-04 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **average Infiltration Rate = 4.3E-04 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA4 - Test 1

Soil Infiltration Rate in Accordance with BR365

Where: V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **990 mm** Average water depth: **255 mm**

Start time = a_{p50} **0 min** Change in water depth: **510 mm**

Final parameters

Depth to water = t_{p75-25} **500 mm** Time interval: **129 min**

End time = **129 min**

Effective Storage Volume of Water in the Trial Pit = **1.02765 m³**
 75% Effective Depth = **1118 mm** from ground level
 25% Effective Depth = **1373 mm** from ground level
 Time at 75% Effective Depth = **27 minutes**
 Time at 25% Effective Depth = **105 minutes**

= **0.51 m³**

= **3.93 m²**

= **6300 sec**

= **2.1E-05 m/sec**

Average Soakaway Rate = **1.3E-04 m³/sec**

Average soakaway area = **3.93 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 2.1E-05 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **average Infiltration Rate = 3.4E-05 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA4 - Test 2

Soil Infiltration Rate in Accordance with BR365

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

V_{p75-25}

Initial parameters

Depth to water = **760 mm** Average water depth: **330 mm**

Start time = a_{p50} **0 min** Change in water depth: **520 mm**

Final parameters

Depth to water = t_{p75-25} **280 mm** Time interval: **98 min**

End time = **98 min**

Effective Storage Volume of Water in the Trial Pit = **1.14855 m³**
 75% Effective Depth = **923 mm** from ground level
 25% Effective Depth = **1208 mm** from ground level
 Time at 75% Effective Depth = **32 minutes**
 Time at 25% Effective Depth = **93 minutes**

= **0.57 m³**

= **4.15 m²**

= **5580 sec**

= **2.5E-05 m/sec**

Average Soakaway Rate = **1.8E-04 m³/sec**

Average soakaway area = **4.49 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 2.5E-05 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **average Infiltration Rate = 4.0E-05 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA5 - Test 1

Soil Infiltration Rate in Accordance with BR365

Where:

V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **1330 mm**
Start time = a_{p50} **0 min**

Average water depth: **235 mm**

Change in water depth: **470 mm**

Final parameters

Depth to water = t_{p75-25} **800 mm**
End time = **63 min**

Time interval: **63 min**

Effective Storage Volume of Water in the Trial Pit = **0.8372 m³**
75% Effective Depth = **1455 mm** from ground level
25% Effective Depth = **1685 mm** from ground level
Time at 75% Effective Depth = **11 minutes**
Time at 25% Effective Depth = **46 minutes**

= **0.42 m³**

= **3.41 m²**

= **2760 sec**

= **4.5E-05 m/sec**

Average Soakaway Rate = **2.3E-04 m³/sec**
Average soakaway area = **3.44 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 4.5E-05 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **average Infiltration Rate = 6.6E-05 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA5 - Test 2

Soil Infiltration Rate in Accordance with BR365

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

Where: V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **1270 mm** Average water depth: **200 mm**
 Start time = **10 min** Change in water depth: **400 mm**

Final parameters

Depth to water = **1670 mm** Time interval: **114 min**
 End time = **124 min**

Effective Storage Volume of Water in the Trial Pit = **0.8008 m³**
 75% Effective Depth = **1340 mm** from ground level
 25% Effective Depth = **1560 mm** from ground level
 Time at 75% Effective Depth = **26 minutes**
 Time at 25% Effective Depth = **109 minutes**

V_{p75-25} = **0.40 m³**
 a_{p50} = **3.34 m²**
 t_{p75-25} = **6540 sec**
 f = **1.8E-05 m/sec**

Average Soakaway Rate = **1.1E-04 m³/sec**
 Average soakaway area = **3.20 m²** (sides + base)

BR365 Soil Infiltration Rate = 1.8E-05 m/sec
Average Infiltration Rate = 3.3E-05 m/sec

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA6 - Test 1

Soil Infiltration Rate in Accordance with BR365

Where:

V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **830 mm** Average water depth: **235 mm**

Start time = a_{p50} **0 min** Change in water depth: **470 mm**

Final parameters

Depth to water = t_{p75-25} **300 mm** Time interval: **14 min**

End time = **14 min**

Effective Storage Volume of Water in the Trial Pit = **0.924 m³**
 75% Effective Depth = **970 mm** from ground level
 25% Effective Depth = **1190 mm** from ground level
 Time at 75% Effective Depth = **4.5 minutes**
 Time at 25% Effective Depth = **9.5 minutes**

= **0.46 m³**

= **3.73 m²**

= **570 sec**

= **2.2E-04 m/sec**

Average Soakaway Rate = **1.2E-03 m³/sec**

Average soakaway area = **3.84 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 2.2E-04 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **average Infiltration Rate = 3.1E-04 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA6 - Test 2

Soil Infiltration Rate in Accordance with BR365

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

V_{p75-25}

Initial parameters

Depth to water = **710 mm** Average water depth: **245 mm**

Start time = a_{p50} **0 min** Change in water depth: **490 mm**

Final parameters

Depth to water = t_{p75-25} **200 mm** Time interval: **24 min**

End time = **24 min**

Effective Storage Volume of Water in the Trial Pit = **0.966 m³**
 75% Effective Depth = **855 mm** from ground level
 25% Effective Depth = **1085 mm** from ground level
 Time at 75% Effective Depth = **6.5 minutes**
 Time at 25% Effective Depth = **18 minutes**

= **0.48 m³**

= **3.80 m²**

= **1080 sec**

= **1.2E-04 m/sec**

Average Soakaway Rate = **7.1E-04 m³/sec**

Average soakaway area = **3.91 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 1.2E-04 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **average Infiltration Rate = 1.8E-04 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
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Test No. SA6 - Test 3

Soil Infiltration Rate in Accordance with BR365

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

V_{p75-25}

Initial parameters

Depth to water = **740 mm** Average water depth: **230 mm**

Start time = a_{p50} **0 min** Change in water depth: **460 mm**

Final parameters

Depth to water = t_{p75-25} **200 mm** Time interval: **26 min**

End time = **26 min**

Effective Storage Volume of Water in the Trial Pit = **0.945 m³**
 75% Effective Depth = **863 mm** from ground level
 25% Effective Depth = **1088 mm** from ground level
 Time at 75% Effective Depth = **7 minutes**
 Time at 25% Effective Depth = **18 minutes**

= **0.47 m³**

= **3.77 m²**

= **1080 sec**

= **1.2E-04 m/sec**

Average Soakaway Rate = **6.2E-04 m³/sec**

Average soakaway area = **3.80 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 1.2E-04 m/sec**

$\frac{V_{p75-25}}{a_{p50}}$ **verage Infiltration Rate = 1.6E-04 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared JA/SAE	Checked DN

Test No. SA7 - Test 1

Soil Infiltration Rate in Accordance with BR365

Where:

V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **680 mm** Average water depth: **260 mm**

Start time = a_{p50} **0 min** Change in water depth: **520 mm**

Final parameters

Depth to water = t_{p75-25} **200 mm** Time interval: **121 min**

End time = **121 min**

Effective Storage Volume of Water in the Trial Pit = **1.24 m³**
 75% Effective Depth = **825 mm** from ground level
 25% Effective Depth = **1075 mm** from ground level
 Time at 75% Effective Depth = **18 minutes**
 Time at 25% Effective Depth = **70 minutes**

= **0.62 m³**

= **4.43 m²**

= **4200 sec**

= **3.3E-05 m/sec**

Average Soakaway Rate = **1.8E-04 m³/sec**

Average soakaway area = **4.51 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 3.3E-05 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **average Infiltration Rate = 3.9E-05 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared SAE	Checked DN

Test No. SA7 - Test 2

Soil Infiltration Rate in Accordance with BR365

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

V_{p75-25}

Initial parameters

Depth to water = **910 mm** Average water depth: **230 mm**

Start time = a_{p50} **10 min** Change in water depth: **320 mm**

Final parameters

Depth to water = t_{p75-25} **230 mm** Time interval: **126 min**

End time = **136 min**

Effective Storage Volume of Water in the Trial Pit = **1.0912 m³**
 75% Effective Depth = **970 mm** from ground level
 25% Effective Depth = **1190 mm** from ground level
 Time at 75% Effective Depth = **34 minutes**
 Time at 25% Effective Depth = **128 minutes**

= **0.55 m³**

= **4.20 m²**

= **7680 sec**

= **1.7E-05 m/sec**

Average Soakaway Rate = **1.0E-04 m³/sec**

Average soakaway area = **4.27 m² (sides + base)**

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$ **Soil Infiltration Rate = 1.7E-05 m/sec**
verage Infiltration Rate = 2.5E-05 m/sec

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
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Test No. SA8 - Test 1

Soil Infiltration Rate in Accordance with BR365

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

V_{p75-25}

Initial parameters

Depth to water = **810 mm** Average water depth: **445 mm**

Start time = a_{p50} **0 min** Change in water depth: **90 mm**

Final parameters

Depth to water = t_{p75-25} **900 mm** Time interval: **236 min**

End time = **236 min**

Effective Storage Volume of Water in the Trial Pit = **1.0752 m³**
 75% Effective Depth = **940 mm** from ground level
 25% Effective Depth = **1180 mm** from ground level
 Time at 75% Effective Depth = **N/A** minutes
 Time at 25% Effective Depth = **N/A** minutes

= **0.54 m³**

= **4.11 m²**

= **0 sec**

= **#DIV/0! m/sec**

Average Soakaway Rate = **1.4E-05 m³/sec**

Average soakaway area = **5.71 m²** (sides + base)

$\frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$ **Soil Infiltration Rate = UTC m/sec**
verage Infiltration Rate = 2.5E-06 m/sec

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
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Test No. SA9 - Test 1

Soil Infiltration Rate in Accordance with BR365

Where:

is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

is the internal surface area of the trial pit up to 50% effective depth and including the base area

is the time for the water level to fall from 75% to 25% effective depth

V_{p75-25}

Initial parameters

Depth to water = **760 mm** Average water depth: **245 mm**

Start time = a_{p50} **0 min** Change in water depth: **490 mm**

Final parameters

Depth to water = t_{p75-25} **250 mm** Time interval: **45 min**

End time = **45 min**

Effective Storage Volume of Water in the Trial Pit = **1.0528 m³**
 75% Effective Depth = **898 mm** from ground level
 25% Effective Depth = **1133 mm** from ground level
 Time at 75% Effective Depth = **3 minutes**
 Time at 25% Effective Depth = **22 minutes**

= **0.53 m³**

= **4.07 m²**

= **1320 sec**

= **9.8E-05 m/sec**

Average Soakaway Rate = **4.1E-04 m³/sec**

Average soakaway area = **4.15 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 9.8E-05 m/sec**

$\frac{V_{p75-25}}{a_{p50}}$ **verage Infiltration Rate = 9.8E-05 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
SUBJECT:	Infiltration Test Results and Calculation of Infiltration Rates	Prepared SAE	Checked DN

Test No. SA9 - Test 2

Soil Infiltration Rate in Accordance with BR365

Where: V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **700 mm** Average water depth: **275 mm**

Start time = a_{p50} **0 min** Change in water depth: **550 mm**

Final parameters

Depth to water = t_{p75-25} **250 mm** Time interval: **62 min**

End time = **62 min**

Effective Storage Volume of Water in the Trial Pit = **1.2096 m³**
 75% Effective Depth = **845 mm** from ground level
 25% Effective Depth = **1115 mm** from ground level
 Time at 75% Effective Depth = **6 minutes**
 Time at 25% Effective Depth = **36 minutes**

= **0.60 m³**

= **4.35 m²**

= **2160 sec**

= **6.4E-05 m/sec**

Average Soakaway Rate = **3.3E-04 m³/sec**

Average soakaway area = **4.39 m²** (sides + base)

$\frac{V_{p75-25}}{t_{p75-25}}$ **Soil Infiltration Rate = 6.4E-05 m/sec**
 $\frac{V_{p75-25}}{a_{p50}}$ **average Infiltration Rate = 7.6E-05 m/sec**

t_{p75-25}

PROJECT:	Wombwell High School	Job No. 43497	Date 19.12.18
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Test No. SA9 - Test 3

Soil Infiltration Rate in Accordance with BR365

$$f = \frac{V_{p75-25}}{a_{p50} \times t_{p75-25}}$$

Where: V_{p75-25} is the effective storage volume of water in the trial pit between 75% and 25% effective depth;

a_{p50} is the internal surface area of the trial pit up to 50% effective depth and including the base area

t_{p75-25} is the time for the water level to fall from 75% to 25% effective depth

Initial parameters

Depth to water = **690** mm Average water depth: **280** mm
 Start time = **0** min Change in water depth: **560** mm

Final parameters

Depth to water = **1250** mm Time interval: **60** min
 End time = **60** min

Effective Storage Volume of Water in the Trial Pit = **1.2096** m³
 75% Effective Depth = **845** mm from ground level
 25% Effective Depth = **1115** mm from ground level
 Time at 75% Effective Depth = **9** minutes
 Time at 25% Effective Depth = **38** minutes

V_{p75-25} = **0.60** m³

a_{p50} = **4.35** m²

t_{p75-25} = **2280** sec

f = **6.1E-05** m/sec

Average Soakaway Rate = **3.5E-04** m³/sec
 Average soakaway area = **4.42** m² (sides + base)

BR365 Soil Infiltration Rate = 6.1E-05 m/sec
Average Infiltration Rate = 7.9E-05 m/sec

End of Report